

ADS5463

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12-Bit, 500-MSPS Analog-to-Digital Converter

FEATURES

- 500-MSPS Sample Rate
- 12-Bit Resolution, 10.4 Bits ENOB
- 2.3-GHz Input Bandwidth
- SFDR = 75 dBc at 450 MHz and 500 MSPS
- SNR = 64.6 dBFS at 450 MHz and 500 MSPS
- 2.2- V_{PP} Differential Input Voltage
- LVDS-Compatible Outputs
- Total Power Dissipation: 2.2 W
- Offset Binary Output Format
- Output Data Transitions on the Rising and Falling Edges of a Half-Rate Output Clock
- On-Chip Analog Buffer, Track and Hold, and Reference Circuit

- 80-Pin TQFP PowerPAD™ Package (14-mm × 14-mm)
- Industrial Temperature Range = -40°C to 85°C
- Pin-Similar/Compatible to 12-, 13-, and 14-Bit Family: ADS5440/ADS5444/ADS5474

APPLICATIONS

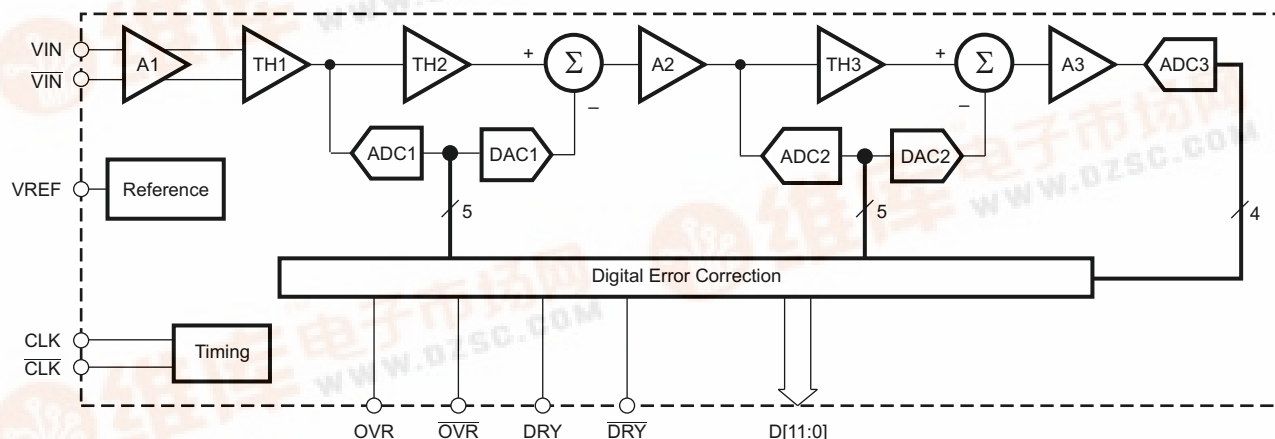
- Test and Measurement Instrumentation
- Software-Defined Radio
- Data Acquisition
- Power Amplifier Linearization
- Communication Instrumentation
- Radar

DESCRIPTION

The ADS5463 is a 12-bit, 500-MSPS analog-to-digital converter (ADC) that operates from both a 5-V supply and 3.3-V supply, while providing LVDS-compatible digital outputs. This ADC is one of a family of 12-, 13-, and 14-bit ADCs that operate from 210 MSPS to 500 MSPS. The ADS5463 input buffer isolates the internal switching of the onboard track and hold (T&H) from disturbing the signal source while providing a high-impedance input. An internal reference generator is also provided to simplify the system design.

Designed with a 2.3-GHz input bandwidth for the conversion of signals that exceed 500MHz of input center frequency at 500 MSPS, the ADS5463 has outstanding low noise performance and spurious-free dynamic range over a large input frequency range.

The ADS5463 is available in a TQFP-80 PowerPAD™ package. The ADS5463 is built on Texas Instrument's complementary bipolar process (BiCom3) and is specified over the full industrial temperature range (-40°C to 85°C).



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This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

PACKAGE/ORDERING INFORMATION

PRODUCT	PACKAGE-LEAD	PACKAGE DESIGNATOR ⁽¹⁾	SPECIFIED TEMPERATURE RANGE	PACKAGE MARKING	ORDERING NUMBER	TRANSPORT MEDIA, QUANTITY
ADS5463	HTQFP-80 ⁽²⁾ PowerPAD	PFP	–40°C to 85°C	ADS5463I	ADS5463IPFP	Tray, 96
					ADS5463IPFPR	Tape and reel, 1000

(1) For the most current product and ordering information, see the Package Option Addendum located at the end of this data sheet.

(2) Thermal pad size: 6.15 mm × 6.15 mm (min), 7.5 mm × 7.5 mm (maximum), see Thermal Pad Addendum located at the end of the data sheet.

ABSOLUTE MAXIMUM RATINGS

over operating free-air temperature range (unless otherwise noted)⁽¹⁾

		ADS5463	UNIT
Supply voltage	AVDD5 to GND	6	V
	AVDD3 to GND	5	V
	DVDD3 to GND	5	V
Analog input to GND	Valid when supplies are on and within normal ranges. See additional information in the Power Supplies portion of the applications information in the back of the datasheet regarding Clock and Analog Inputs when the supplies are off.	–0.3 to (AVDD5 + 0.3)	V
Clock input to GND		–0.3 to (AVDD5 + 0.3)	V
CLK to $\overline{\text{CLK}}$		±2.5	V
Digital data output to GND		–0.3 to (DVDD3 + 0.3)	V
Operating temperature range		–40 to 85	°C
Maximum junction temperature		150	°C
Storage temperature range		–65 to 150	°C
ESD, human-body model (HBM)		2	kV

(1) Stresses above these ratings may cause permanent damage. Exposure to absolute maximum conditions for extended periods may degrade device reliability. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those specified is not implied. Kirkendall voidings and current density information for calculation of expected lifetime is available upon request.

THERMAL CHARACTERISTICS⁽¹⁾

PARAMETER	TEST CONDITIONS	TYP	UNIT
⁽²⁾ R _{θJA}	Soldered thermal pad, no airflow	23.7	°C/W
	Soldered thermal pad, 150-LFM airflow	17.8	
	Soldered thermal pad, 250-LFM airflow	16.4	
⁽³⁾ R _{θJP}	Bottom of package (thermal pad)	2.99	°C/W

(1) Using 36 thermal vias (6 × 6 array). See [PowerPAD Package](#) in the *Application Information* section.

(2) R_{θJA} is the thermal resistance from the junction to ambient.

(3) R_{θJP} is the thermal resistance from the junction to the thermal pad.

RECOMMENDED OPERATING CONDITIONS

	MIN	TYP	MAX	UNIT
SUPPLIES				
AVDD5 Analog supply voltage	4.75	5	5.25	V
AVDD3 Analog supply voltage	3	3.3	3.6	V
DVDD3 Output driver supply voltage	3	3.3	3.6	V
ANALOG INPUT				
Differential input range		2.2		V _{pp}
VCM Input common mode		2.4		V
DIGITAL OUTPUT (DRY, DATA, OVR)				
Maximum differential output load		10		pF
CLOCK INPUT (CLK)				
CLK input sample rate (sine wave)	20		500	MSPS
Clock amplitude, differential sine wave	0.5		5	V _{pp}
Clock duty cycle	40	50	60	%
T _A Open free-air temperature	–40		85	°C

ELECTRICAL CHARACTERISTICS

Typical values at T_A = 25°C, minimum and maximum values over full temperature range T_{MIN} = –40°C to T_{MAX} = 85°C, sampling rate = 500 MSPS, 50% clock duty cycle, AVDD5 = 5 V, AVDD3 = 3.3 V, DVDD3 = 3.3 V, –1-dBFS differential input, and 3-V_{pp} differential clock (unless otherwise noted)

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
Resolution			12		Bits
ANALOG INPUTS					
Differential input range			2.2		V _{PP}
VCM Analog Input common-mode voltage	Self-biased		2.4		V
Input resistance (dc)	Each input to VCM		500		Ω
Input capacitance	Each input to GND (including package)		4.8		pF
Analog input bandwidth (–3 dB)			2.3		GHz
CMRR Common-mode rejection ratio	Common mode signal = 10 MHz		90		dB
INTERNAL REFERENCE VOLTAGE					
V _{REF} Reference voltage			2.4		V
DYNAMIC ACCURACY					
No missing codes		Specified			
DNL Differential linearity error	f _{IN} = 10 MHz	–0.95	±0.25	0.95	LSB
INL Integral linearity error	f _{IN} = 10 MHz	–2.5	+0.8/–0.3	2.5	LSB
Offset error		–11		11	mV
Offset temperature coefficient			0.0005		mV/°C
Gain error		–5		5	%FS
Gain temperature coefficient			–0.02		%FS/°C
POWER SUPPLY					
I _{AVDD5} 5-V analog supply current	V _{IN} = full scale, f _{IN} = 10 MHz, f _S = 500 MSPS		300	330	mA
I _{AVDD3} 3.3-V analog supply current			125	138	mA
I _{DVDD3} 3.3-V digital supply current (includes LVDS)			82	88	mA
Total power dissipation			2.18	2.4	W
Power-up time			200		μs
PSRR Power-supply rejection ratio	Without 0.1-μF board supply capacitors, with 100-kHz supply noise		85		dB

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ELECTRICAL CHARACTERISTICS (continued)

Typical values at $T_A = 25^\circ\text{C}$, minimum and maximum values over full temperature range $T_{\text{MIN}} = -40^\circ\text{C}$ to $T_{\text{MAX}} = 85^\circ\text{C}$, sampling rate = 500 MSPS, 50% clock duty cycle, AVDD5 = 5 V, AVDD3 = 3.3 V, DVDD3 = 3.3 V, -1-dBFS differential input, and 3- V_{PP} differential clock (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
DYNAMIC AC CHARACTERISTICS						
SNR	Signal-to-noise ratio	$f_{\text{IN}} = 10 \text{ MHz}$		65.4		dBFS
		$f_{\text{IN}} = 70 \text{ MHz}$		65.4		
		$f_{\text{IN}} = 100 \text{ MHz}$	63.5	65.3		
		$f_{\text{IN}} = 230 \text{ MHz}$		65.1		
		$f_{\text{IN}} = 300 \text{ MHz}$	63	65		
		$f_{\text{IN}} = 450 \text{ MHz}$		64.6		
		$f_{\text{IN}} = 650 \text{ MHz}$		63.9		
		$f_{\text{IN}} = 900 \text{ MHz}$		62.6		
		$f_{\text{IN}} = 1.3 \text{ GHz}$		59.3		
SFDR	Spurious-free dynamic range	$f_{\text{IN}} = 10 \text{ MHz}$		85		dBc
		$f_{\text{IN}} = 70 \text{ MHz}$		82		
		$f_{\text{IN}} = 100 \text{ MHz}$	70	82		
		$f_{\text{IN}} = 230 \text{ MHz}$		78		
		$f_{\text{IN}} = 300 \text{ MHz}$	64	77		
		$f_{\text{IN}} = 450 \text{ MHz}$		75		
		$f_{\text{IN}} = 650 \text{ MHz}$		65		
		$f_{\text{IN}} = 900 \text{ MHz}$		56		
		$f_{\text{IN}} = 1.3 \text{ GHz}$		45		
HD2	Second harmonic	$f_{\text{IN}} = 10 \text{ MHz}$		87		dBc
		$f_{\text{IN}} = 70 \text{ MHz}$		82		
		$f_{\text{IN}} = 100 \text{ MHz}$	70	80		
		$f_{\text{IN}} = 230 \text{ MHz}$		81		
		$f_{\text{IN}} = 300 \text{ MHz}$	64	77		
		$f_{\text{IN}} = 450 \text{ MHz}$		80		
		$f_{\text{IN}} = 650 \text{ MHz}$		77		
		$f_{\text{IN}} = 900 \text{ MHz}$		66		
		$f_{\text{IN}} = 1.3 \text{ GHz}$		50		
HD3	Third harmonic	$f_{\text{IN}} = 10 \text{ MHz}$		85		dBc
		$f_{\text{IN}} = 70 \text{ MHz}$		90		
		$f_{\text{IN}} = 100 \text{ MHz}$	70	87		
		$f_{\text{IN}} = 230 \text{ MHz}$		90		
		$f_{\text{IN}} = 300 \text{ MHz}$	64	80		
		$f_{\text{IN}} = 450 \text{ MHz}$		75		
		$f_{\text{IN}} = 650 \text{ MHz}$		65		
		$f_{\text{IN}} = 900 \text{ MHz}$		56		
		$f_{\text{IN}} = 1.3 \text{ GHz}$		45		

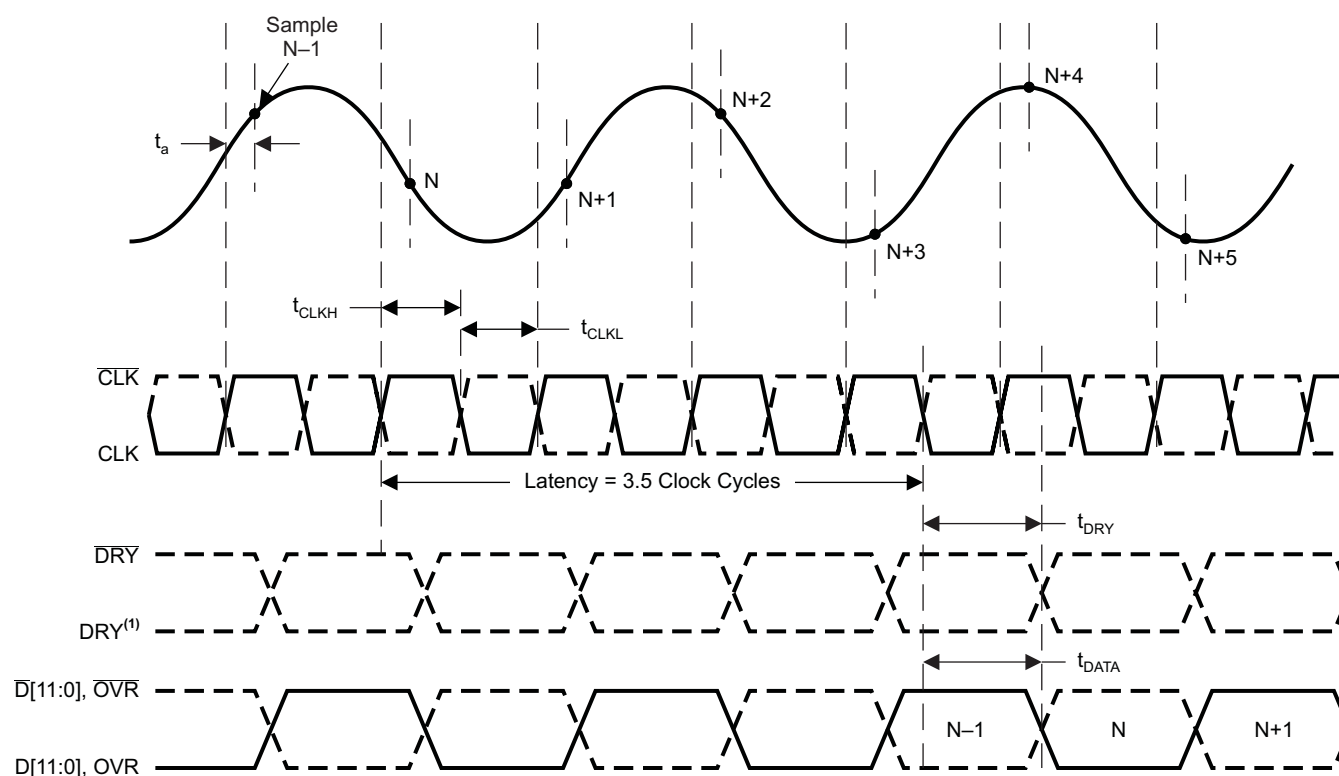
ELECTRICAL CHARACTERISTICS (continued)

Typical values at $T_A = 25^\circ\text{C}$, minimum and maximum values over full temperature range $T_{\text{MIN}} = -40^\circ\text{C}$ to $T_{\text{MAX}} = 85^\circ\text{C}$, sampling rate = 500 MSPS, 50% clock duty cycle, AVDD5 = 5 V, AVDD3 = 3.3 V, DVDD3 = 3.3 V, -1-dBFS differential input, and 3- V_{PP} differential clock (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
DYNAMIC AC CHARACTERISTICS (continued)						
Worst harmonic/spur (other than HD2 and HD3)		$f_{\text{IN}} = 10 \text{ MHz}$		86		dBc
		$f_{\text{IN}} = 70 \text{ MHz}$		86		
		$f_{\text{IN}} = 100 \text{ MHz}$		86		
		$f_{\text{IN}} = 230 \text{ MHz}$		77		
		$f_{\text{IN}} = 300 \text{ MHz}$		81		
		$f_{\text{IN}} = 450 \text{ MHz}$		86		
		$f_{\text{IN}} = 650 \text{ MHz}$		85		
		$f_{\text{IN}} = 900 \text{ MHz}$		78		
		$f_{\text{IN}} = 1.3 \text{ GHz}$		67		
THD Total Harmonic Distortion		$f_{\text{IN}} = 10 \text{ MHz}$		80		dBc
		$f_{\text{IN}} = 70 \text{ MHz}$		79		
		$f_{\text{IN}} = 100 \text{ MHz}$		77		
		$f_{\text{IN}} = 230 \text{ MHz}$		75		
		$f_{\text{IN}} = 300 \text{ MHz}$		73		
		$f_{\text{IN}} = 450 \text{ MHz}$		73		
		$f_{\text{IN}} = 650 \text{ MHz}$		64		
		$f_{\text{IN}} = 900 \text{ MHz}$		55		
		$f_{\text{IN}} = 1.3 \text{ GHz}$		44		
SINAD Signal-to-noise and distortion		$f_{\text{IN}} = 10 \text{ MHz}$		64.2		dBc
		$f_{\text{IN}} = 70 \text{ MHz}$		64.2		
		$f_{\text{IN}} = 100 \text{ MHz}$	62	64.1		
		$f_{\text{IN}} = 230 \text{ MHz}$		63.7		
		$f_{\text{IN}} = 300 \text{ MHz}$		63.5		
		$f_{\text{IN}} = 450 \text{ MHz}$		63.1		
		$f_{\text{IN}} = 650 \text{ MHz}$		60.5		
		$f_{\text{IN}} = 900 \text{ MHz}$		54.4		
		$f_{\text{IN}} = 1.3 \text{ GHz}$		44.1		
Two-tone SFDR		$f_{\text{IN1}} = 65 \text{ MHz}$, $f_{\text{IN2}} = 70 \text{ MHz}$, each tone at -7 dBFS		90		dBFS
		$f_{\text{IN1}} = 65 \text{ MHz}$, $f_{\text{IN2}} = 70 \text{ MHz}$, each tone at -16 dBFS		89		
		$f_{\text{IN1}} = 350 \text{ MHz}$, $f_{\text{IN2}} = 355 \text{ MHz}$, each tone at -7 dBFS		82		
		$f_{\text{IN1}} = 350 \text{ MHz}$, $f_{\text{IN2}} = 355 \text{ MHz}$, each tone at -16 dBFS		89		
ENOB Effective number of bits		$f_{\text{IN}} = 100 \text{ MHz}$	10	10.4		Bits
		$f_{\text{IN}} = 300 \text{ MHz}$		10.4		
RMS idle-channel noise		Inputs tied to common-mode		0.7		LSB
LVDS DIGITAL OUTPUTS						
V_{OD}	Differential output voltage (\pm)		247	350	454	mV
V_{OC}	Common mode output voltage		1.125		1.375	V

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(1) Polarity of DRY is undetermined. For further information, see the [Digital Outputs](#) section.

Figure 1. Timing Diagram

TIMING CHARACTERISTICS⁽¹⁾

Typical values at $T_A = 25^\circ\text{C}$, Min and Max values over full temperature range $T_{\text{MIN}} = -40^\circ\text{C}$ to $T_{\text{MAX}} = 85^\circ\text{C}$, sampling rate = 500 MSPS, 50% clock duty cycle, AVDD5 = 5 V, AVDD3 = 3.3 V, DVDD3 = 3.3 V, and $3-V_{\text{PP}}$ differential clock (unless otherwise noted)

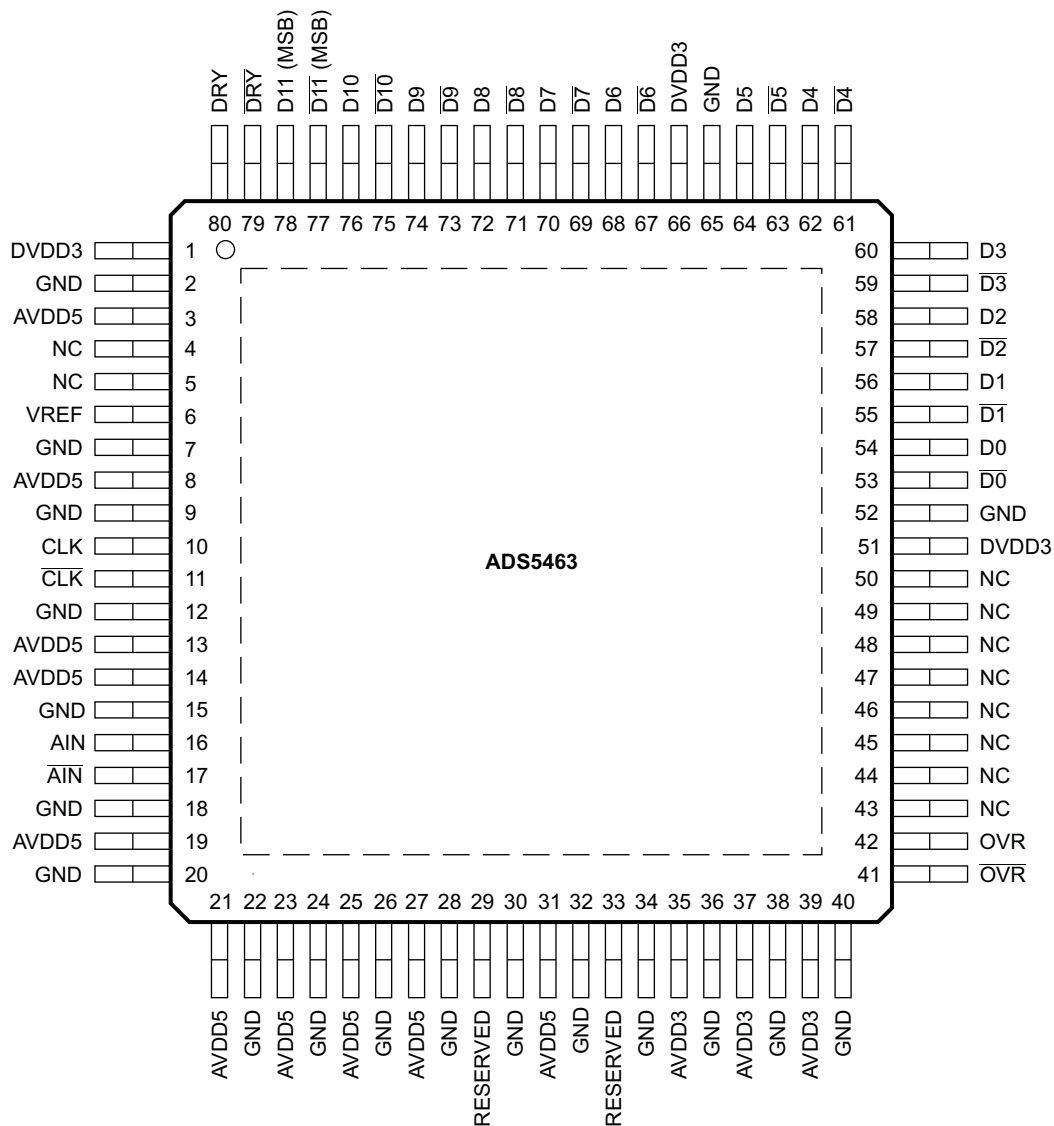
PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
t _a	Aperture delay		200			ps
	Aperture jitter, rms		150			fs
	Latency		3.5			cycles
t _{CLK}	Clock period		2		50	ns
t _{CLKH}	Clock pulse duration, high		1			ns
t _{CLKL}	Clock pulse duration, low		1			ns
t _{DRY}	CLK to DRY delay ⁽²⁾	Zero crossing, 10-pF parasitic loading to GND on each output pin	950		1600	ps
t _{DATA}	CLK to DATA/OVR delay ⁽²⁾	Zero crossing, 10-pF parasitic loading to GND on each output pin	750		2100	ps
t _{SKEW}	DATA to DRY skew	t _{DATA} – t _{DRY} , 10-pF parasitic loading to GND on each output pin	–350	0	650	ps
t _{RISE}	DRY/DATA/OVR rise time	10-pF parasitic loading to GND on each output pin	500			ps
t _{FALL}	DRY/DATA/OVR fall time	10-pF parasitic loading to GND on each output pin	500			ps

(1) Timing parameters are specified by design or characterization, but not production tested.

(2) DRY, DATA, and OVR are updated on the falling edge of CLK. The latency must be added to t_{DATA} to determine the overall propagation delay.

PIN CONFIGURATION

**PFP PACKAGE
(TOP VIEW)**



P0027-02

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Table 1. TERMINAL FUNCTIONS

TERMINAL		DESCRIPTION
NAME	NO.	
AIN	16	Differential input signal (positive)
$\overline{\text{AIN}}$	17	Differential input signal (negative)
AVDD5	3, 8, 13, 14, 19, 21, 23, 25, 27, 31	Analog power supply (5 V)
AVDD3	35, 37, 39	Analog power supply (3.3 V) (Suggestion for ≤ 250 MSPS: leave option to connect to 5 V for ADS5440/4 13-bit compatibility)
DVDD3	1, 51, 66	Output driver power supply (3.3 V)
GND	2, 7, 9, 12, 15, 18, 20, 22, 24, 26, 28, 30, 32, 34, 36, 38, 40, 52, 65	Ground
CLK	10	Differential input clock (positive). Conversion is initiated on rising edge.
$\overline{\text{CLK}}$	11	Differential input clock (negative)
D0, $\overline{\text{D0}}$	54, 53	LVDS digital output pair, least-significant bit (LSB)
D1–D10, $\overline{\text{D1}}\text{--}\overline{\text{D10}}$	55–64, 67–76	LVDS digital output pairs
D11, $\overline{\text{D11}}$	78, 77	LVDS digital output pair, most-significant bit (MSB)
DRY, $\overline{\text{DRY}}$	80, 79	Data ready LVDS output pair
NC	4, 5, 43–50	No connect (4 and 5 should be left floating, 43–50 are possible future bit additions for this pinout and therefore can be connected to a digital bus or left floating)
OVR, $\overline{\text{OVR}}$	42, 41	Overrange indicator LVDS output. A logic high signals an analog input in excess of the full-scale range.
RESERVED	29, 33	Pin 29 is reserved for possible future Vcm output for this pinout, like ADS5474; pin 33 is reserved for possible future power-down control pin for this pinout, like ADS5474.
VREF	6	Reference voltage input/output (2.4V nominal)

TYPICAL CHARACTERISTICS

Typical plots at $T_A = 25^\circ\text{C}$, sampling rate = 500 MSPS, 50% clock duty cycle, AVDD5 = 5 V, AVDD3 = 3.3 V, DVDD3 = 3.3 V, and 3- V_{PP} differential clock, (unless otherwise noted)

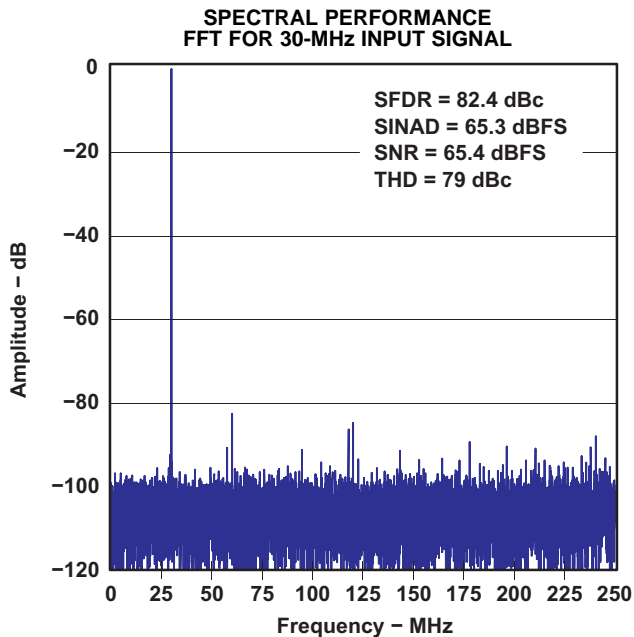


Figure 2.

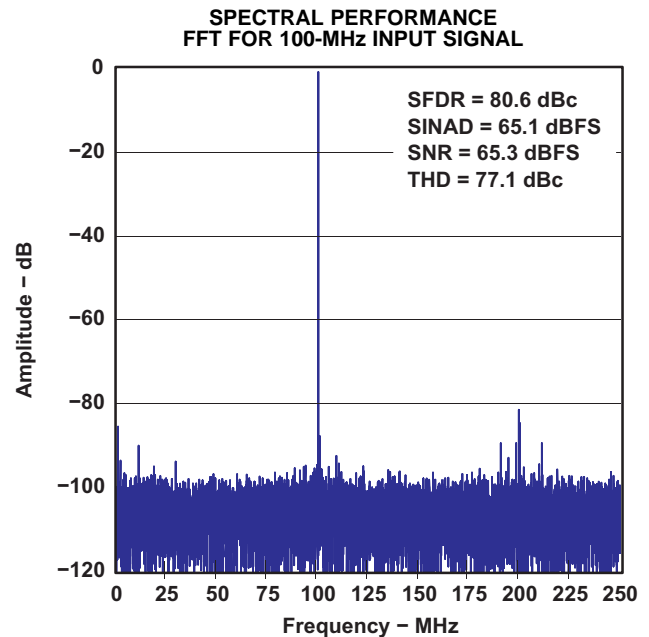


Figure 3.

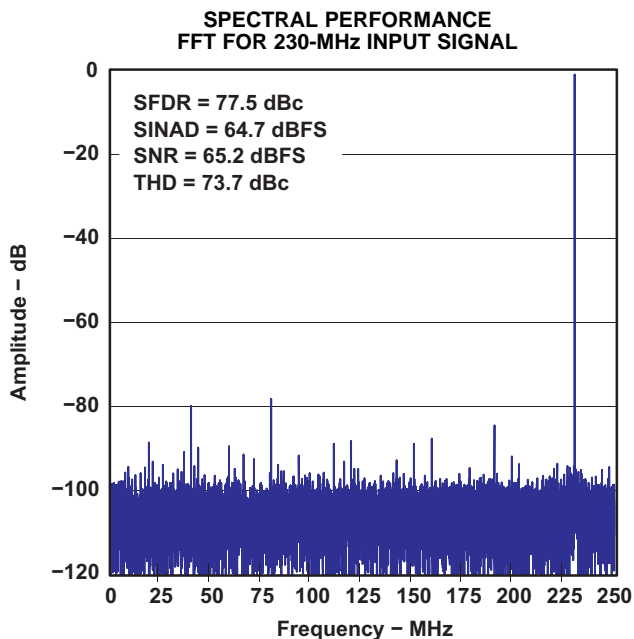


Figure 4.

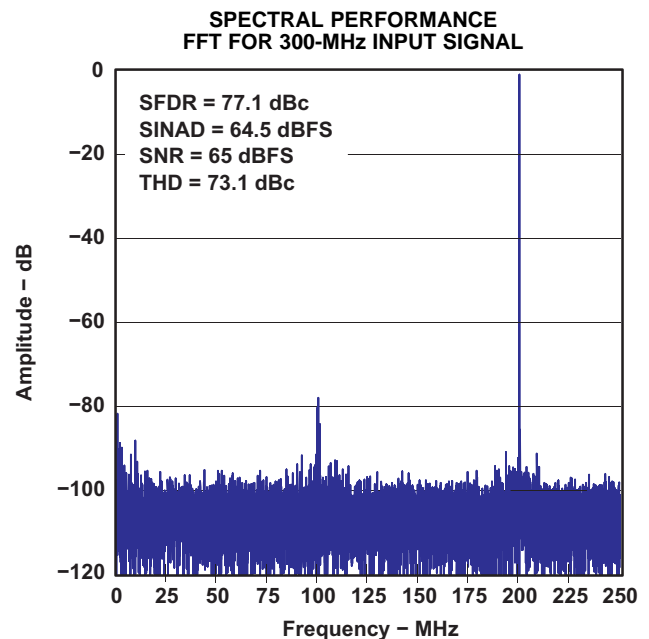


Figure 5.

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TYPICAL CHARACTERISTICS (continued)

Typical plots at $T_A = 25^\circ\text{C}$, sampling rate = 500 MSPS, 50% clock duty cycle, AVDD5 = 5 V, AVDD3 = 3.3 V, DVDD3 = 3.3 V, and 3- V_{PP} differential clock, (unless otherwise noted)

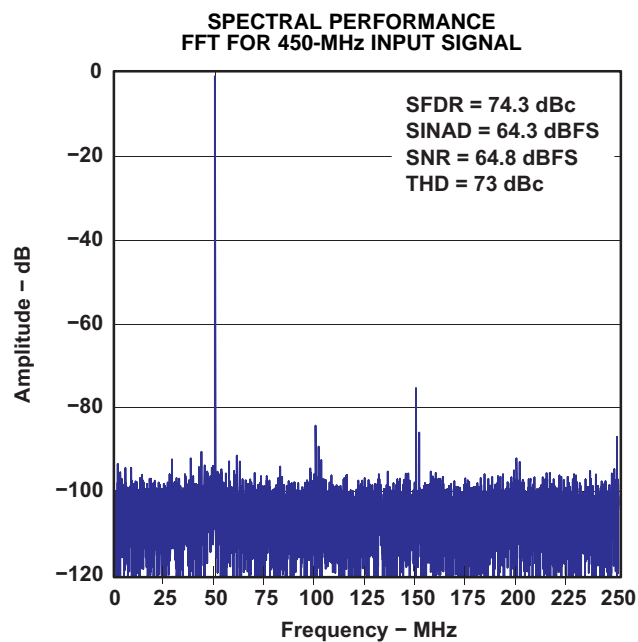


Figure 6.

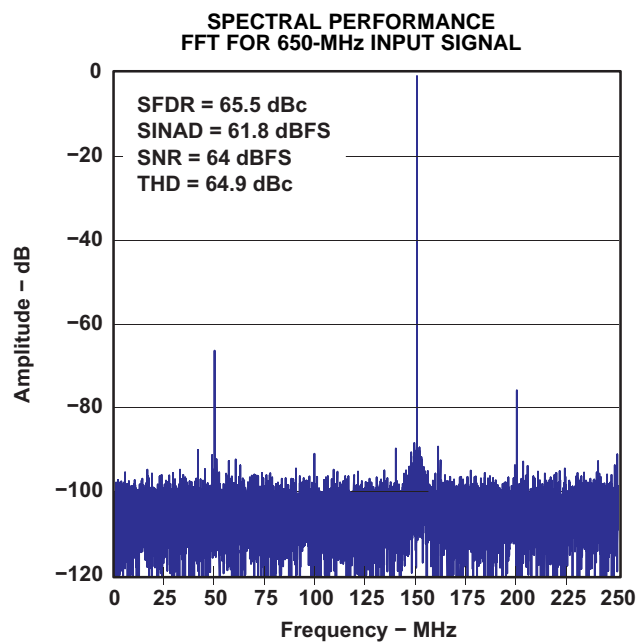


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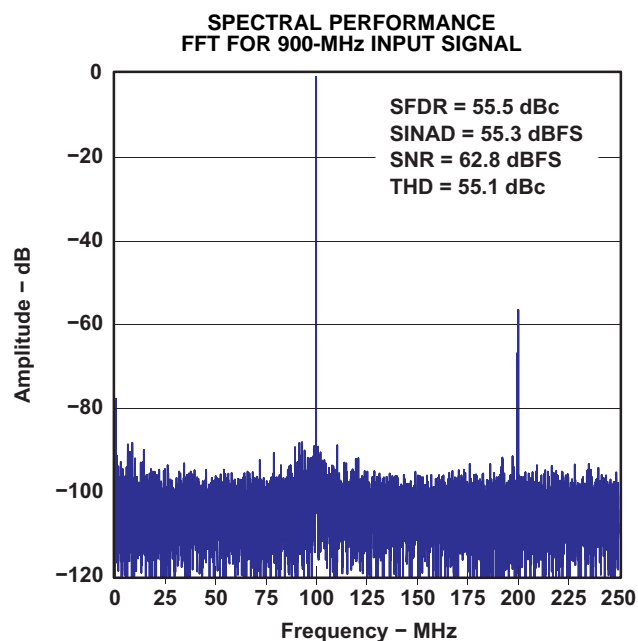


Figure 8.

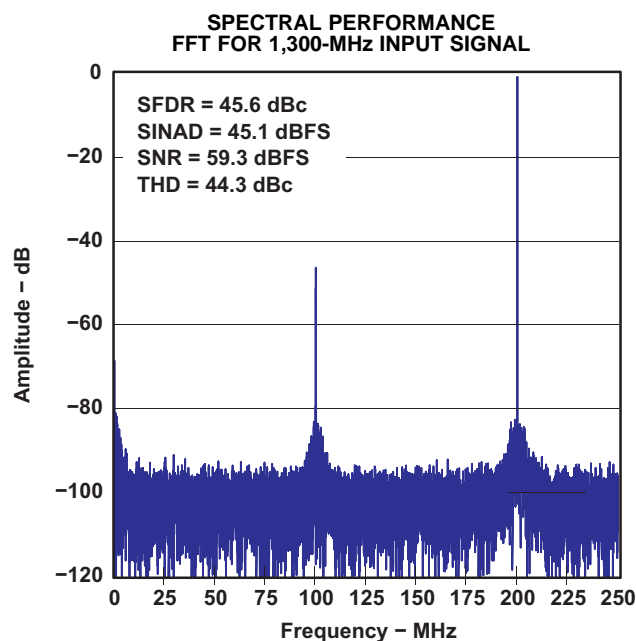


Figure 9.

TYPICAL CHARACTERISTICS (continued)

Typical plots at $T_A = 25^\circ\text{C}$, sampling rate = 500 MSPS, 50% clock duty cycle, AVDD5 = 5 V, AVDD3 = 3.3 V, DVDD3 = 3.3 V, and 3- V_{PP} differential clock, (unless otherwise noted)

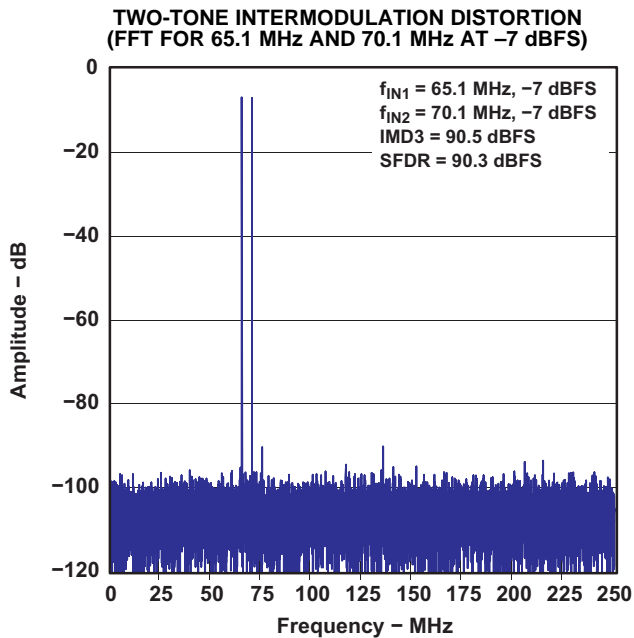


Figure 10.

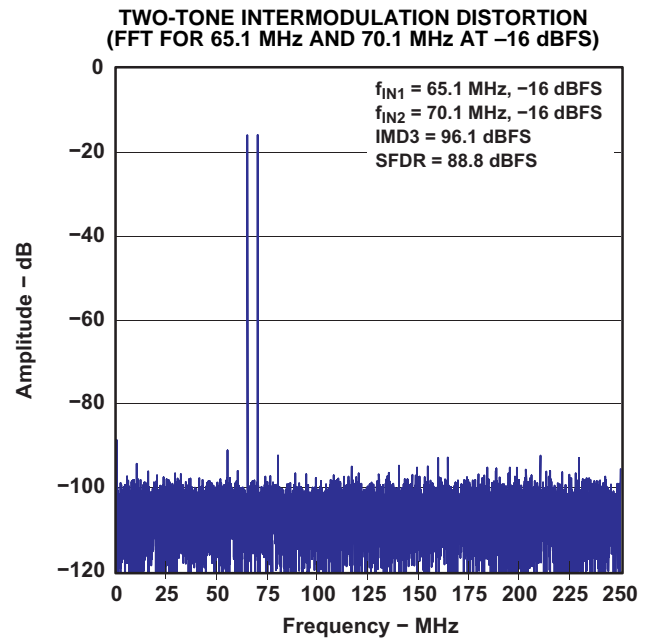


Figure 11.

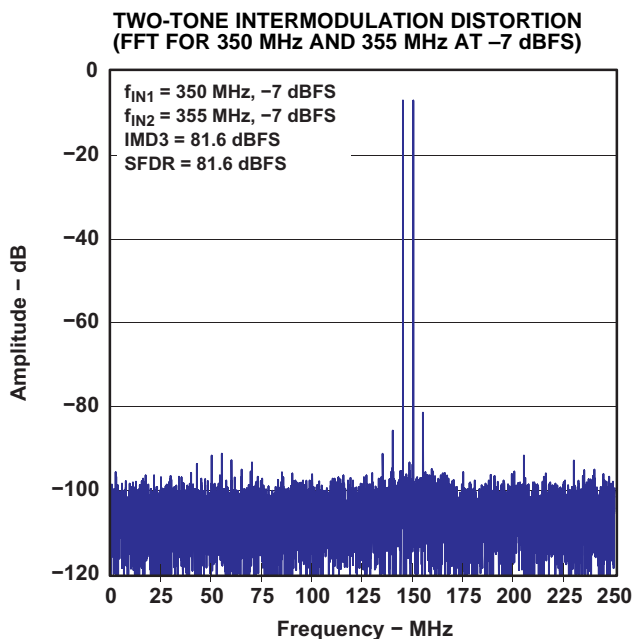


Figure 12.

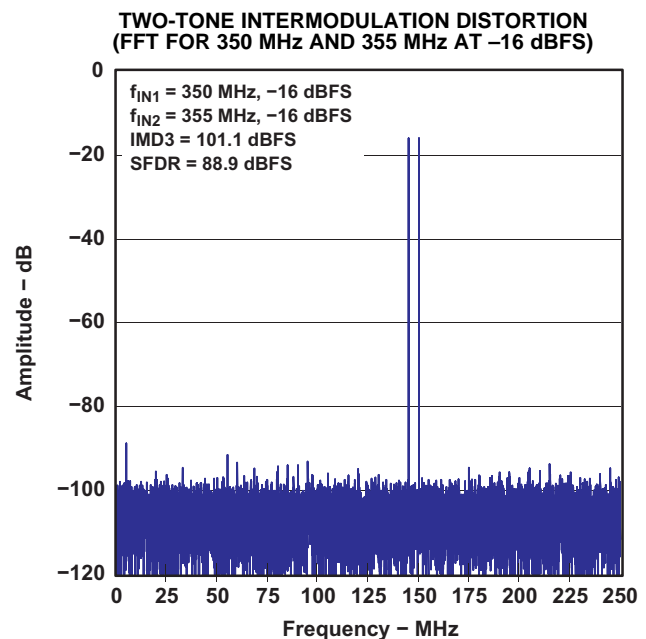


Figure 13.

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TYPICAL CHARACTERISTICS (continued)

Typical plots at $T_A = 25^\circ\text{C}$, sampling rate = 500 MSPS, 50% clock duty cycle, AVDD5 = 5 V, AVDD3 = 3.3 V, DVDD3 = 3.3 V, and 3- V_{PP} differential clock, (unless otherwise noted)

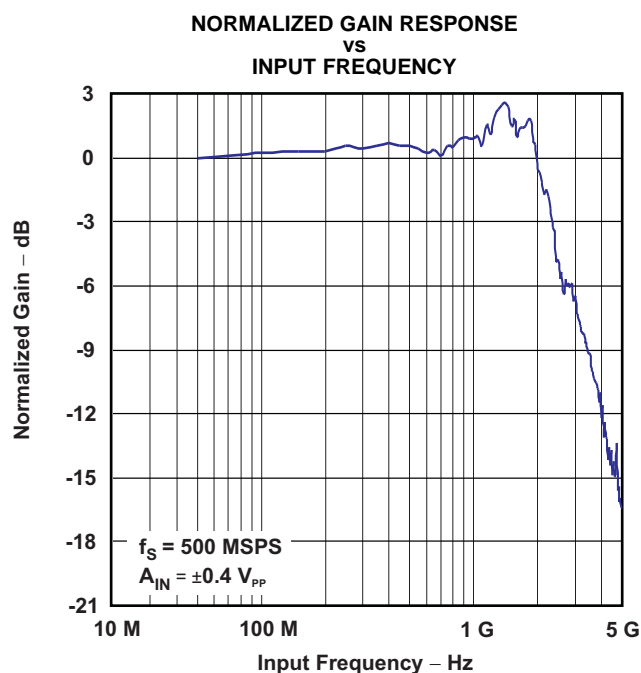


Figure 14.

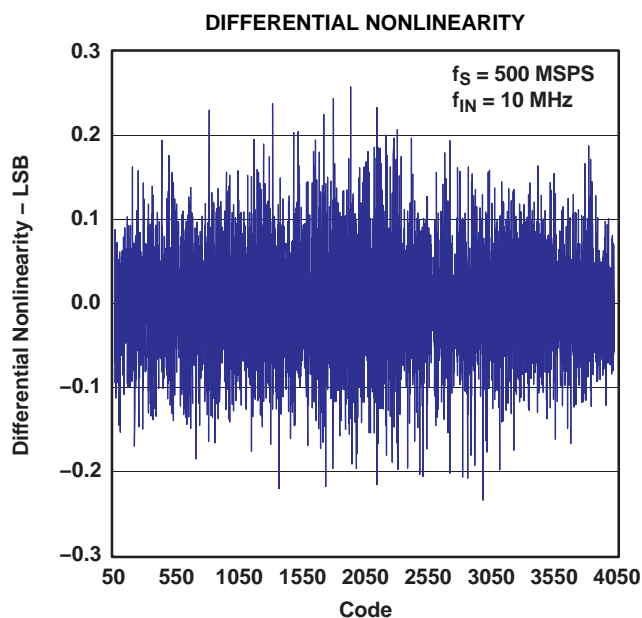


Figure 15.

G014

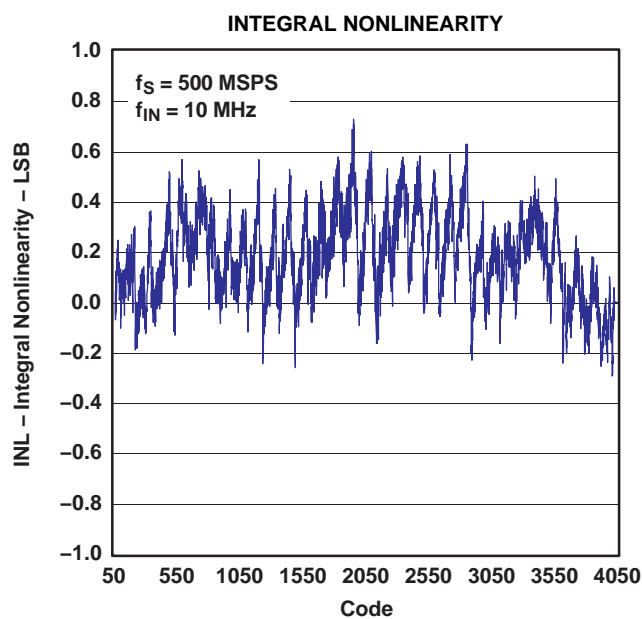


Figure 16.

G015

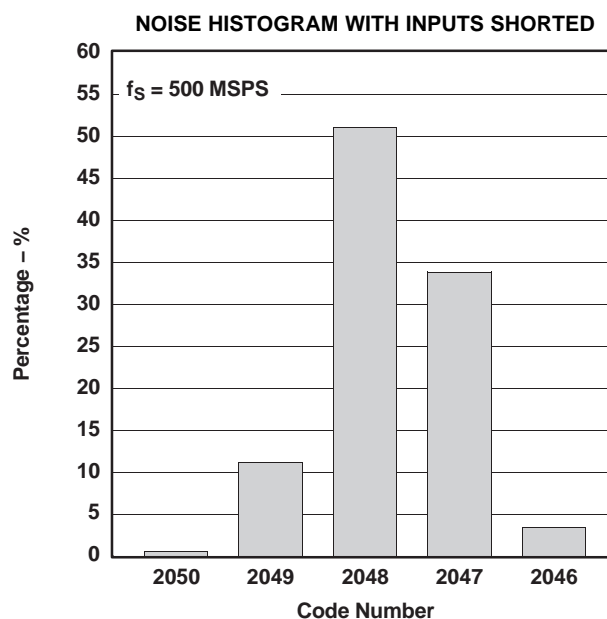


Figure 17.

G016

TYPICAL CHARACTERISTICS (continued)

Typical plots at $T_A = 25^\circ\text{C}$, sampling rate = 500 MSPS, 50% clock duty cycle, $AV_{DD5} = 5\text{ V}$, $AV_{DD3} = 3.3\text{ V}$, $DV_{DD3} = 3.3\text{ V}$, and 3- V_{PP} differential clock, (unless otherwise noted)

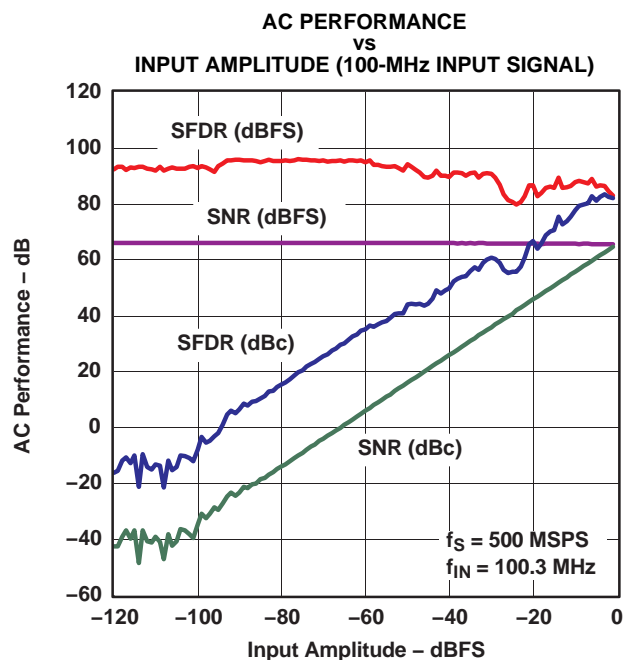


Figure 18.

G017

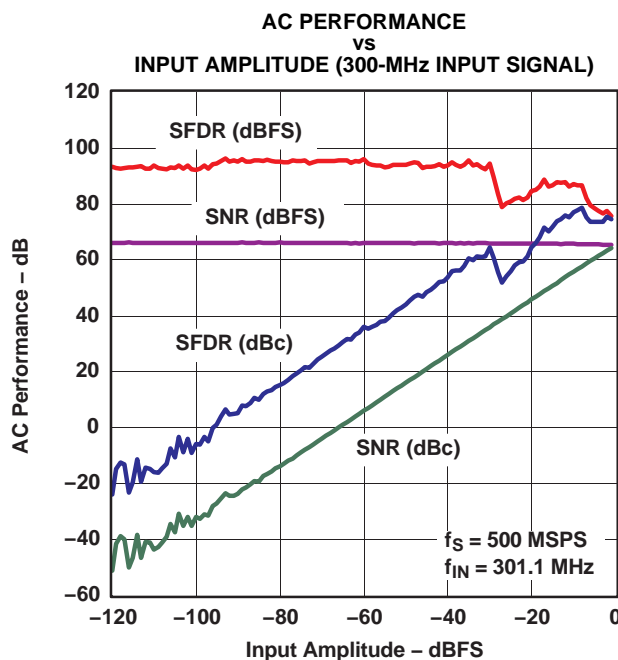


Figure 19.

G018

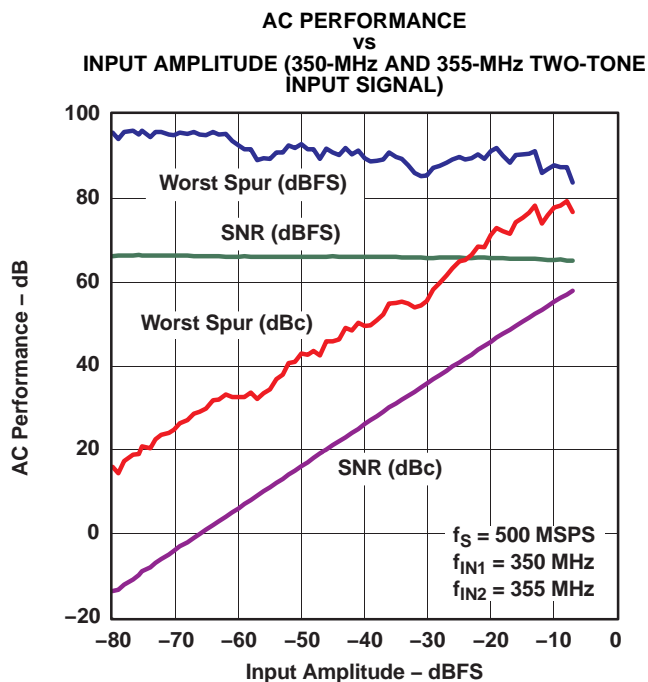


Figure 20.

G020

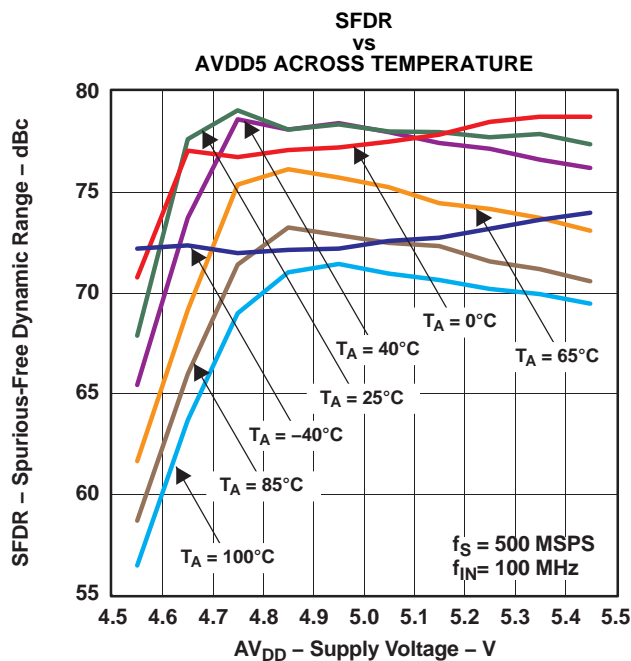
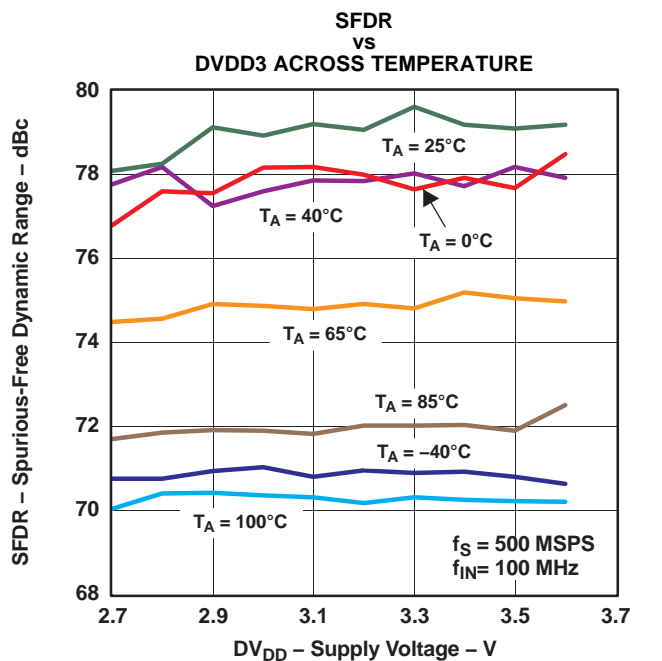
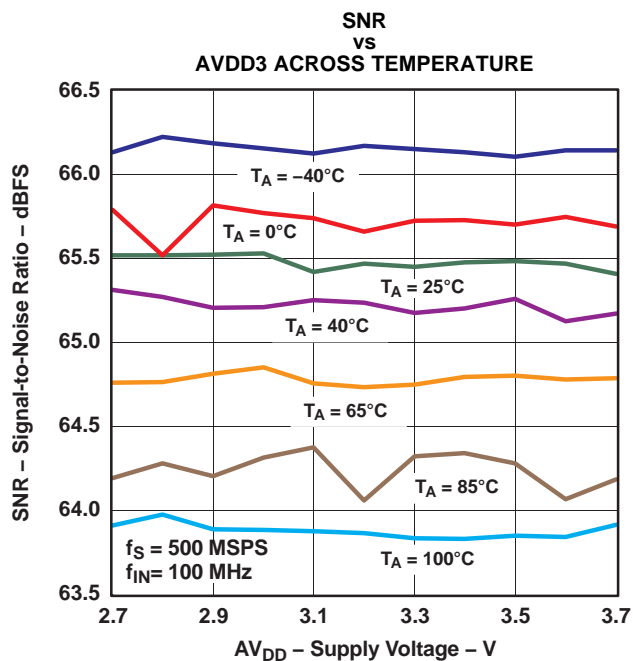
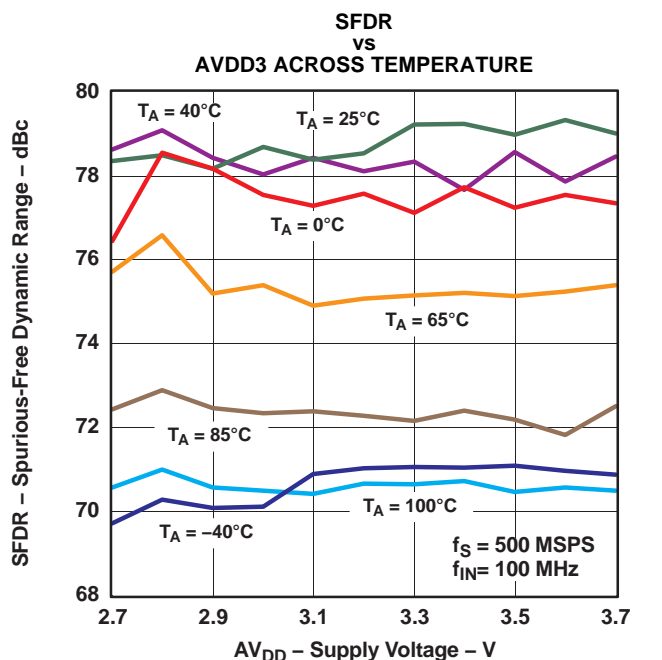
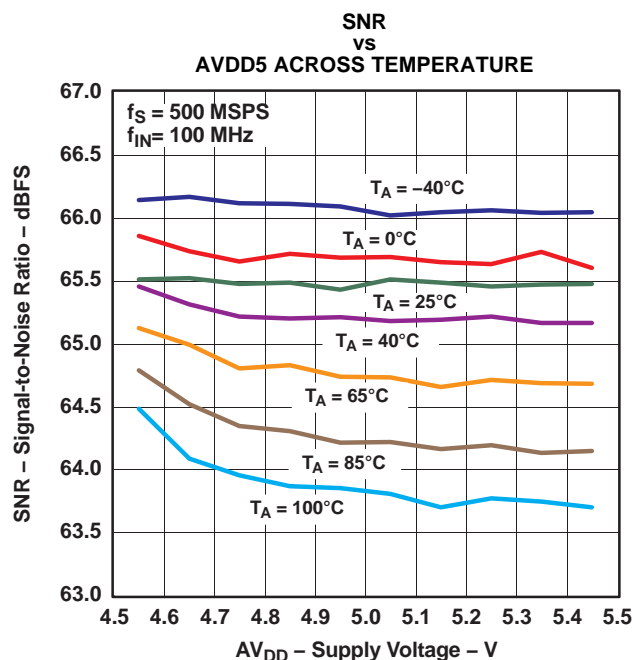


Figure 21.

G026

TYPICAL CHARACTERISTICS (continued)

Typical plots at $T_A = 25^\circ\text{C}$, sampling rate = 500 MSPS, 50% clock duty cycle, AVDD5 = 5 V, AVDD3 = 3.3 V, DVDD3 = 3.3 V, and 3- V_{PP} differential clock, (unless otherwise noted)



TYPICAL CHARACTERISTICS (continued)

Typical plots at $T_A = 25^\circ\text{C}$, sampling rate = 500 MSPS, 50% clock duty cycle, AVDD5 = 5 V, AVDD3 = 3.3 V, DVDD3 = 3.3 V, and 3- V_{PP} differential clock, (unless otherwise noted)

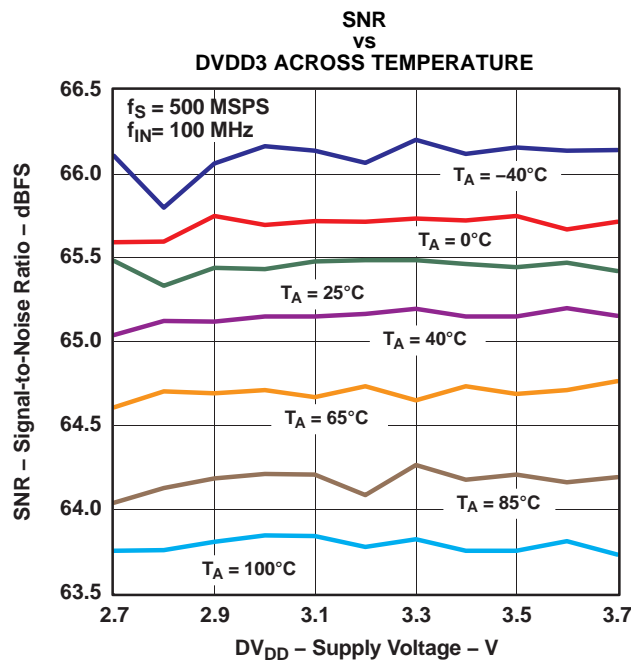


Figure 26.

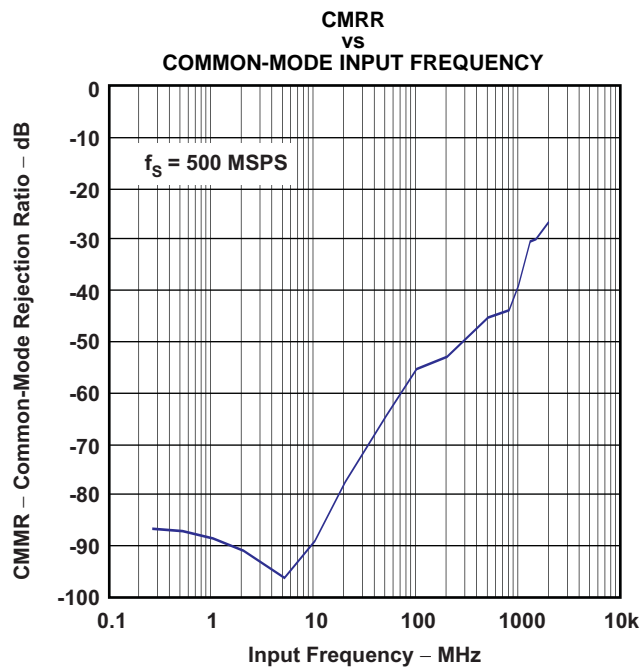


Figure 27.

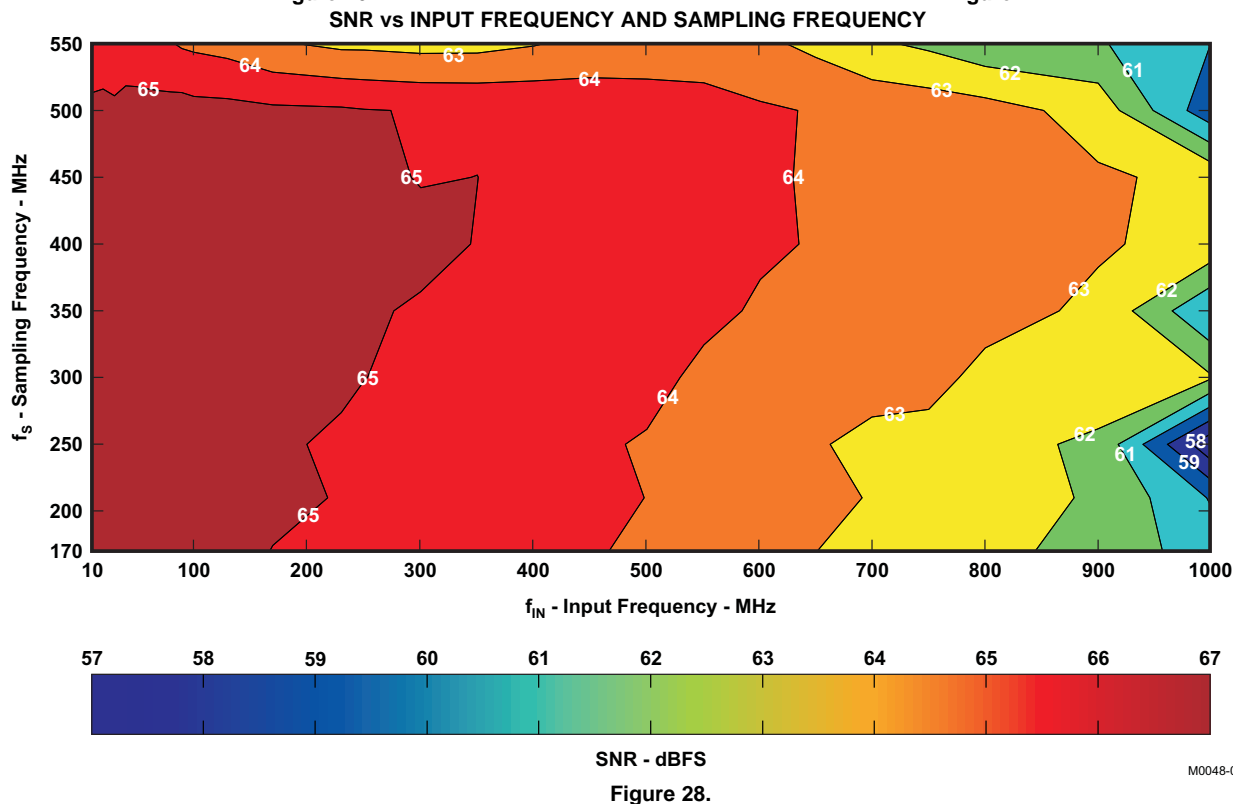


Figure 28.

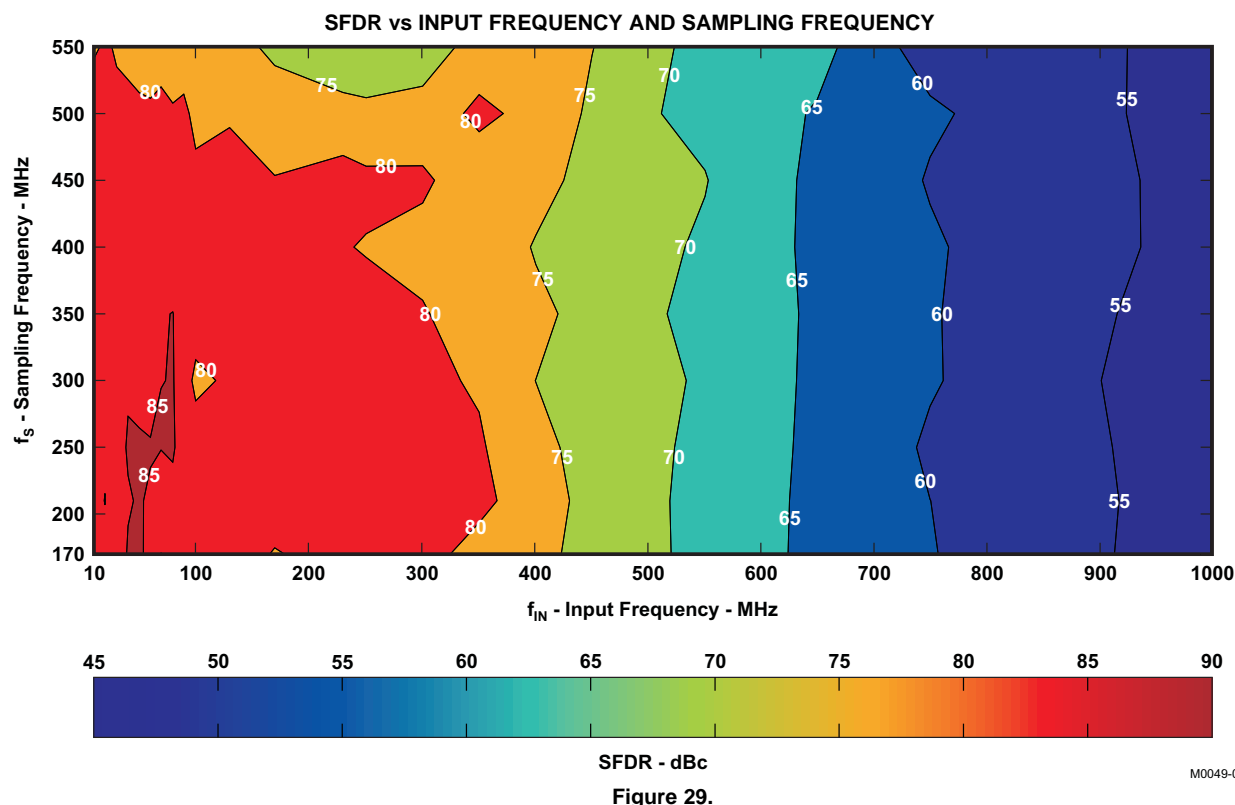
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TYPICAL CHARACTERISTICS (continued)

Typical plots at $T_A = 25^\circ\text{C}$, sampling rate = 500 MSPS, 50% clock duty cycle, AVDD5 = 5 V, AVDD3 = 3.3 V, DVDD3 = 3.3 V, and 3- V_{PP} differential clock, (unless otherwise noted)



APPLICATION INFORMATION

Theory of Operation

The ADS5463 is a 12-bit, 500-MSPS, monolithic pipeline ADC. Its bipolar analog core operates from 5-V and 3.3-V supplies, while the output uses a 3.3-V supply to provide LVDS-compatible outputs. The conversion process is initiated by the rising edge of the external input clock. At that instant, the differential input signal is captured by the input track-and-hold (T&H), and the input sample is sequentially converted by a series of lower resolution stages, with the outputs combined in a digital correction logic block. Both the rising and the falling clock edges are used to propagate the sample through the pipeline every half clock cycle. This process results in a data latency of 3.5 clock cycles, after which the output data is available as a 12-bit parallel word, coded in offset binary format.

Input Configuration

The analog input for the ADS5463 consists of an analog pseudo-differential buffer followed by a bipolar transistor track-and-hold (see [Figure 30](#)). The analog buffer isolates the source driving the input of the ADC from any internal switching and presents a high impedance that is easy to drive at high input frequencies, compared to an ADC without a buffered input. The input common mode is set internally through a 500- Ω resistor connected from 2.4 V to each of the inputs. This results in a differential input impedance of 1 k Ω .

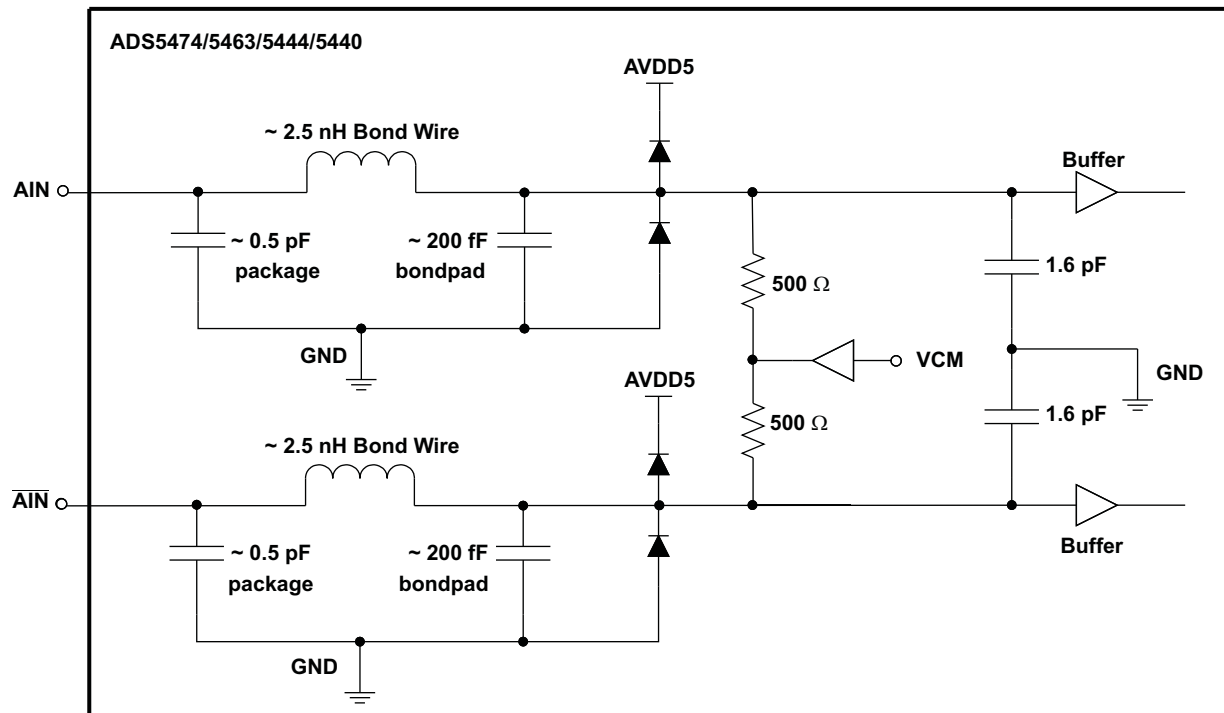
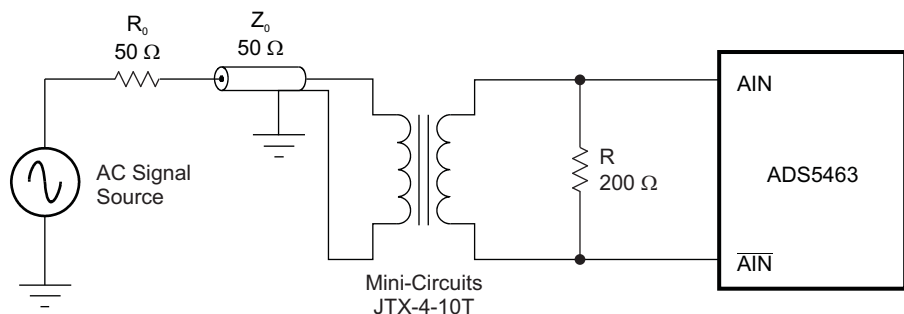


Figure 30. Analog Input Equivalent Circuit

For a full-scale differential input, each of the differential lines of the input signal (pins 16 and 17) swing symmetrically between $2.4\text{ V} + 0.55\text{ V}$ and $2.4\text{ V} - 0.55\text{ V}$. This means that each input has a maximum signal swing of 1.1 V_{PP} for a total differential input signal swing of 2.2 V_{PP} . Operation below 2.2 V_{PP} is allowable, with the characteristics of performance versus input amplitude demonstrated in [Figure 18](#) and [Figure 19](#). For instance, for performance at 1.1 V_{PP} rather than 2.2 V_{PP} , see the SNR and SFDR at -6 dBFS (0 dBFS = 2.2 V_{PP}). The maximum swing is determined by the internal reference voltage generator, eliminating the need for any external circuitry for this purpose.

The ADS5463 obtains optimum performance when the analog inputs are driven differentially. The circuit in [Figure 31](#) shows one possible configuration using an RF transformer with termination either on the primary or on the secondary of the transformer. In addition, the evaluation module is configured with two back-to-back transformers, which also demonstrates good performance. If voltage gain is required, a step-up transformer can be used.



S0176-03

Figure 31. Converting a Single-Ended Input to a Differential Signal Using an RF Transformer

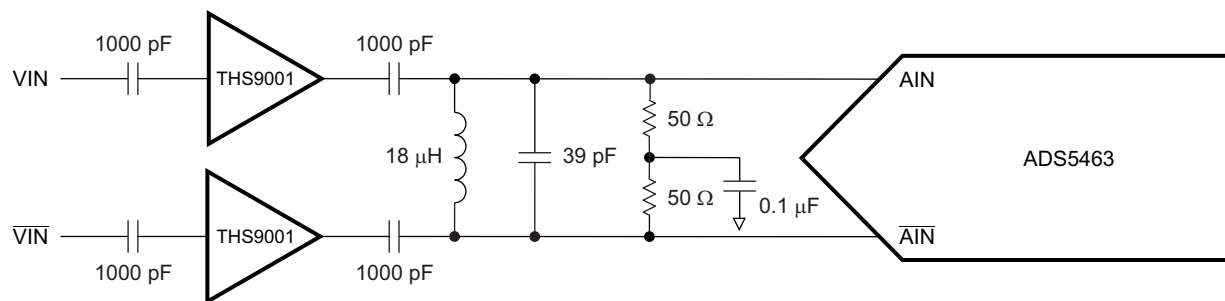
In addition to the transformer configurations, Texas Instruments offers a wide selection of single-ended operational amplifiers that can be selected depending on the application. An RF gain-block amplifier, such as the Texas Instruments THS9001, can also be used for high-input-frequency applications. For large voltage gains at

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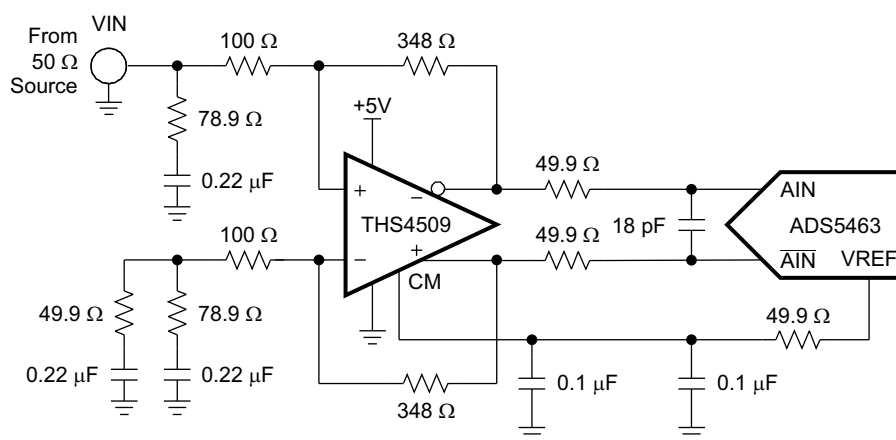
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intermediate-frequencies in the 50-MHz–350-MHz range, the configuration shown in [Figure 32](#) can be used. The component values can be tuned for different intermediate frequencies. The example shown is located on the evaluation module and is tuned for an IF of 170 MHz. More information regarding this configuration can be found in the *ADS5463 EVM User Guide* ([SLAU194](#)) and the *THS9001 50 MHz to 350 MHz Cascadeable Amplifier* data sheet ([SLOS426](#)).



S0177-03

Figure 32. Using the THS9001 IF Amplifier With the ADS5463



S0193-02

Figure 33. Using the THS4509 With the ADS5463

For applications requiring dc-coupling with the signal source, a differential input/differential output amplifier like the THS4509 (see [Figure 33](#)) provides good harmonic performance and low noise over a wide range of frequencies. Notice that VREF is used for the common mode with the ADS5463 and ADS5444/5440, whereas VCM must be used with the ADS5474.

In this configuration, the THS4509 amplifier circuit provides 10 dB of gain, converts the single-ended input to differential, and sets the proper input common-mode voltage to the ADS5463 by using the VREF pin from the ADC. The 50-Ω resistors and 18-pF capacitor between the THS4509 outputs and ADS5463 inputs (along with the input capacitance of the ADC) limit the bandwidth of the signal to about 70 MHz (–3 dB). Input termination is accomplished via the 78.9-Ω resistor and 0.22-µF capacitor to ground, in conjunction with the input impedance of the amplifier circuit. A 0.22-µF capacitor and 49.9-Ω resistor are inserted to ground across the 78.9-Ω resistor and 0.22-µF capacitor on the alternate input to balance the circuit. Gain is a function of the source impedance, termination, and 348-Ω feedback resistor. See the THS4509 data sheet for further component values to set proper 50-Ω termination for other common gains. Because the ADS5463 recommended input common-mode voltage is 2.4 V, the THS4509 is operated from a single power supply input with V S+ = 5 V and V S– = 0 V (ground). This maintains maximum headroom on the internal transistors of the THS4509.

External Voltage Reference

For systems that require the analog signal gain to be adjusted or calibrated, this can be performed by using an external reference. The dependency on the signal amplitude to the value of the external reference voltage is characterized typically by [Figure 34](#) (VREF = 2.4 V is normalized to 0 dB as this is the internal reference voltage. This figure is the average gain adjustment from the data collected from -1dBFS to -6dBFS in 1 dB steps.) As can be seen in the linear fit, this equates to approximately -0.3 dB of signal adjustment per 100 mV of reference adjustment. The range of allowable variation depends on the analog input amplitude that is applied to the inputs and the desired spectral performance, as can be seen in the performance versus external reference graphs in [Figure 35](#) and [Figure 36](#). As the applied analog signal amplitude is reduced, more variation in the reference voltage is allowed in the positive direction (which equates to a reduction in signal amplitude), whereas an adjustment in reference voltage below the nominal 2.4 V (which equates to an increase in signal amplitude) is not recommended below approximately 2.35 V. The power consumption versus reference voltage and operating temperature should also be considered, especially at high ambient temperatures, because the lifetime of the device is affected by internal junction temperature, see [Figure 49](#).

The ADS5463 does not have a VCM output pin and primarily uses the VREF pin to provide the common-mode voltage in dc-coupled applications. The ADS5463 (VCM = 2.4 V) and [ADS5474](#) (VCM = 3.1 V) do not have the same common-mode voltage, but they do share the same approximate VREF (2.4 V). To create a board layout that may accommodate both devices in dc-coupled applications, route the VCM of the ADS5474 and the VREF of the ADS5463 both to a common point that can be selected via a switch, jumper, or a 0 Ω resistor to be used as the common-mode voltage of the driving circuit.

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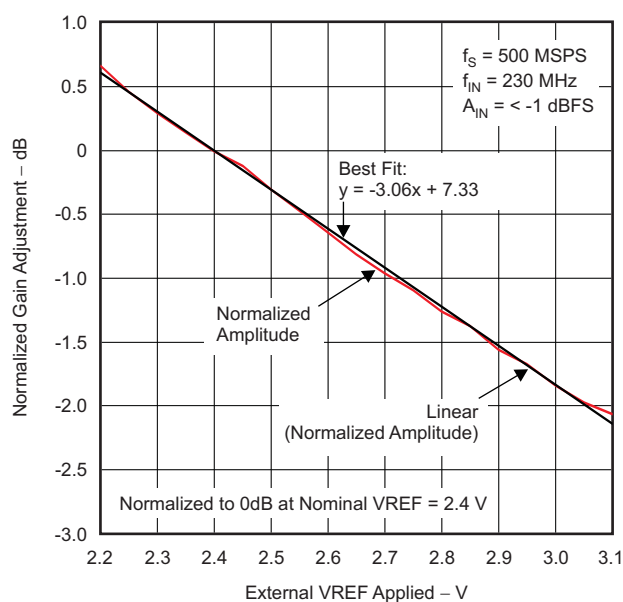


Figure 34. Signal Gain Adjustment versus External Reference (VREF)

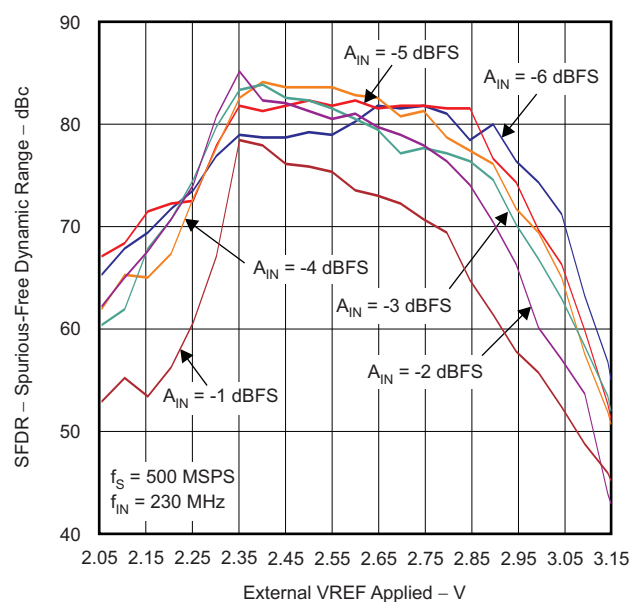


Figure 35. SFDR versus External VREF and A_{IN}

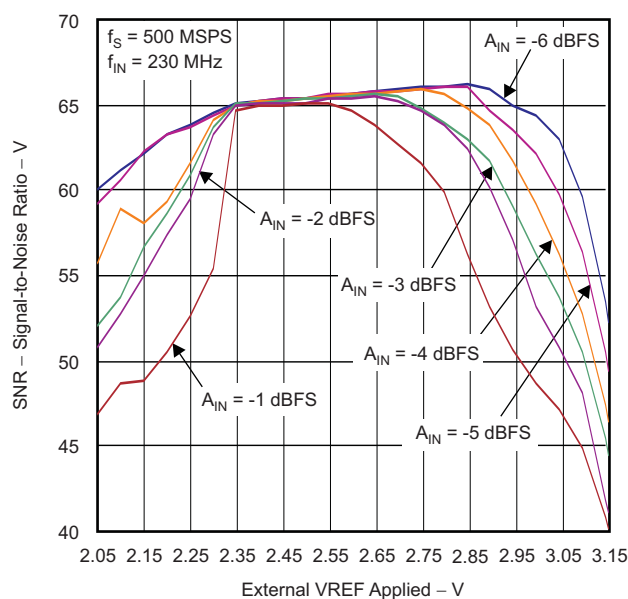


Figure 36. SNR versus External VREF and A_{IN}

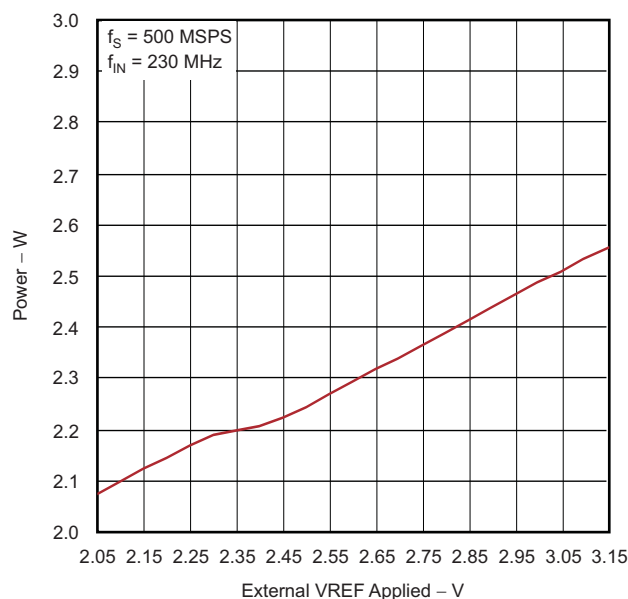


Figure 37. Total Power Consumption versus External VREF

Clock Inputs

The ADS5463 clock input can be driven with either a differential clock signal or a single-ended clock input. The equivalent clock input circuit can be seen in Figure 38. In low-input-frequency applications, where jitter may not be a big concern, the use of a single-ended clock (as shown in Figure 39) could save cost and board space without much performance tradeoff. When clocked with this configuration, it is best to connect $\overline{\text{CLK}}$ to ground with a 0.01- μF capacitor, while CLK is ac-coupled with a 0.01- μF capacitor to the clock source, as shown in Figure 39.

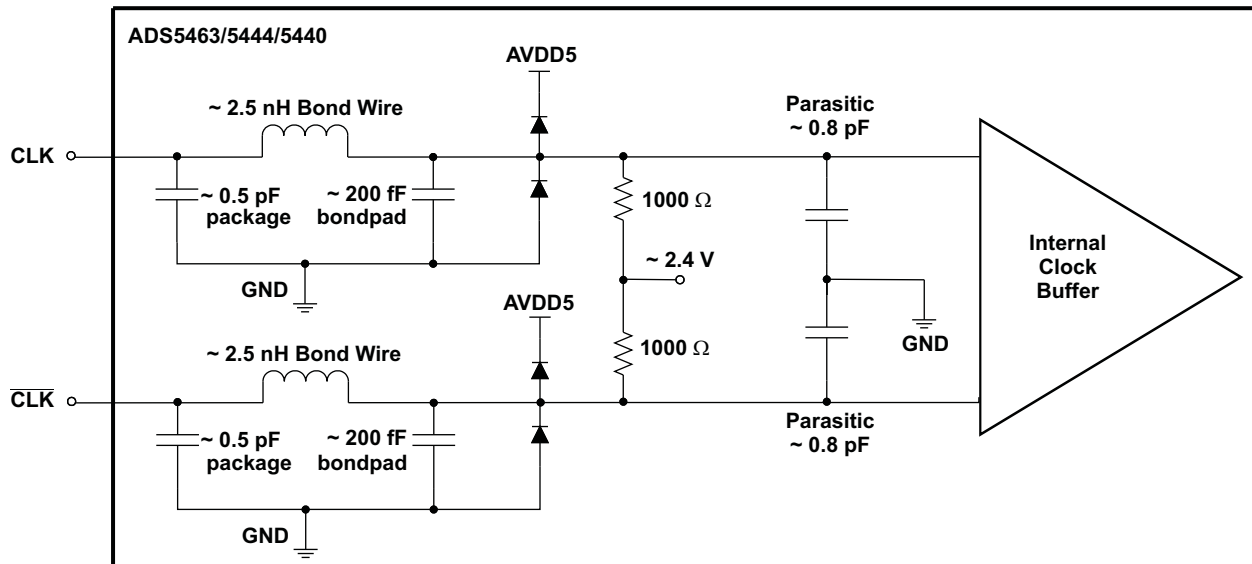
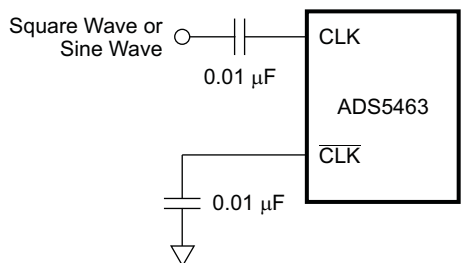


Figure 38. Clock Input Circuit



S0168-05

Figure 39. Single-Ended Clock

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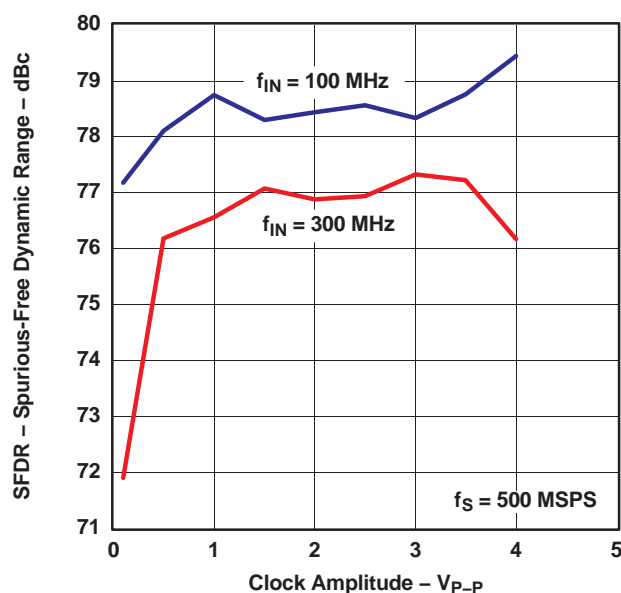


Figure 40. SFDR versus Differential Clock Level

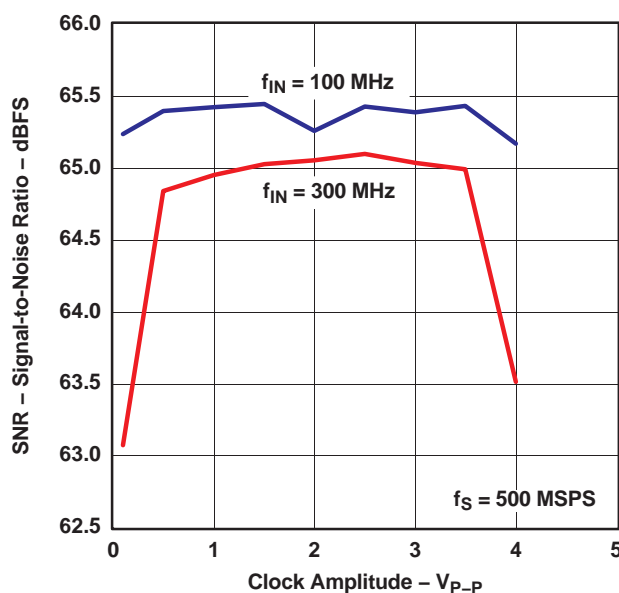


Figure 41. SNR versus Differential Clock Level

The characterization of the ADS5463 is typically performed with a 3- V_{PP} differential clock, but the ADC performs well with a differential clock amplitude down to $\sim 0.5 V_{PP}$ (250mV swing on both CLK and $\overline{\text{CLK}}$), as shown in [Figure 40](#) and [Figure 41](#). For jitter-sensitive applications, the use of a differential clock has some advantages at the system level. The differential clock allows for common-mode noise rejection at the printed circuit board (PCB) level. With a differential clock, the signal-to-noise ratio of the ADC is better for jitter-sensitive, high-frequency applications because the board level clock jitter is superior.

Larger clock amplitude levels are recommended for high analog input frequencies or slow clock frequencies. At high analog input frequencies, the sampling process is sensitive to jitter. At slow clock frequencies, a small amplitude sinusoidal clock has a lower slew rate and can create jitter-related SNR degradation due to the uncertainty in the sampling point associated with a slow slew rate. [Figure 42](#) demonstrates a recommended method for converting a single-ended clock source into a differential clock; it is similar to the configuration found on the evaluation board and was used for much of the characterization. See also *Clocking High Speed Data Converters* ([SLYT075](#)) for more details.

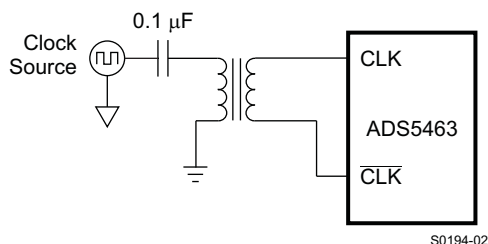


Figure 42. Differential Clock

The common-mode voltage of the clock inputs is set internally to 2.4 V using internal 1-k Ω resistors (see [Figure 38](#)). It is recommended to use ac coupling, but if this scheme is not possible, the ADS5474 features good tolerance to clock common-mode variation, as shown in [Figure 43](#) and [Figure 44](#). The internal ADC core uses both edges of the clock for the conversion process. Ideally, a 50% duty-cycle clock signal should be provided, though even 40/60 is good enough for many applications. Performance degradation as a result of duty cycle can be seen in [Figure 45](#).

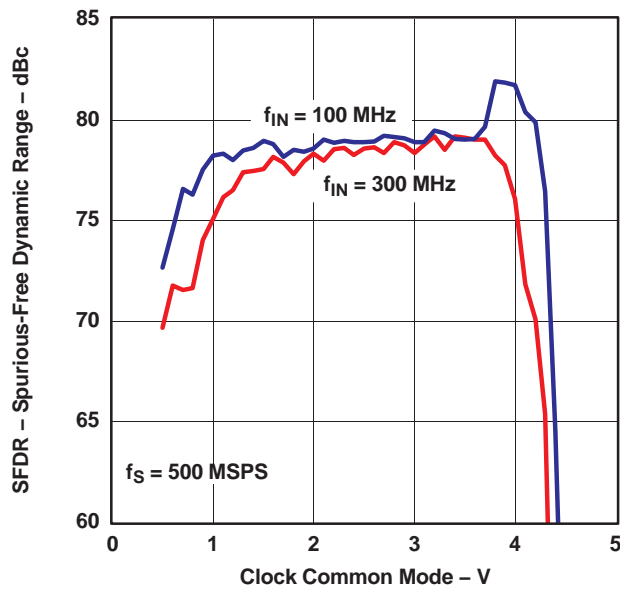


Figure 43. SFDR versus Clock Common Mode

G024

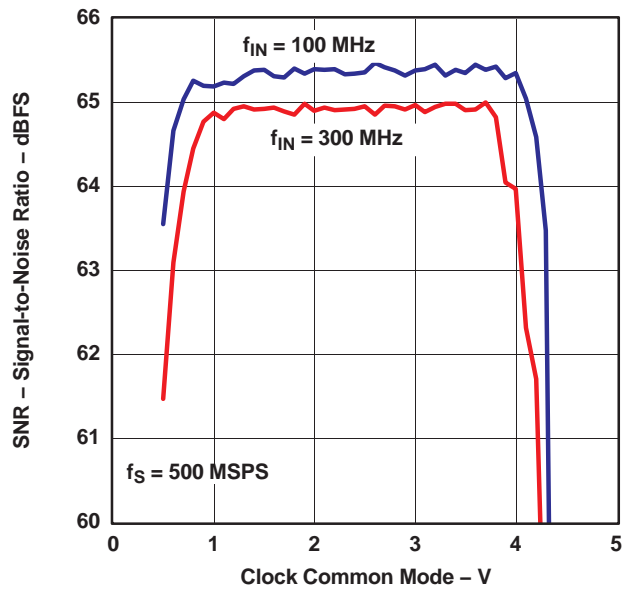


Figure 44. SNR versus Clock Common Mode

G025

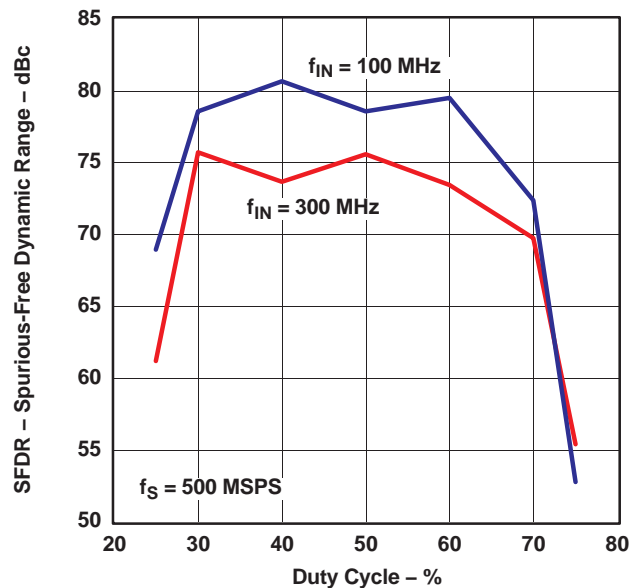


Figure 45. SFDR vs Clock Duty Cycle

G021

To understand how to determine the required clock jitter, an example is useful. The ADS5463 is capable of achieving 63.6 dBFS SNR at 450 MHz of analog input frequency. In order to achieve this SNR at 450 MHz the clock source rms jitter must be at least 181 fsec when combined with the 150 fsec of internal aperture jitter in order for the total rms jitter to be 234 fsec. A summary of maximum recommended rms clock jitter as a function of analog input frequency is provided in [Table 2](#) (using 150 fsec of internal aperture jitter). The equations used to create the table are also presented.

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Table 2. Recommended RMS Clock Jitter

INPUT FREQUENCY (MHz)	MEASURED SNR (dBc)	TOTAL JITTER (fsec rms)	MAXIMUM CLOCK JITTER (fsec rms)
10	64.4	9590	9589
70	64.4	1370	1362
100	64.3	970	959
230	64.1	432	405
300	64	335	300
450	63.6	234	181
650	62.9	175	94
1300	58.3	149	16

Equation 1 and Equation 2 are used to estimate the required clock source jitter.

$$\text{SNR (dBc)} = -20 \times \text{LOG}_{10} (2 \times \pi \times f_{\text{IN}} \times j_{\text{TOTAL}}) \quad (1)$$

$$j_{\text{TOTAL}} = (j_{\text{ADC}}^2 + j_{\text{CLOCK}}^2)^{1/2} \quad (2)$$

where:

j_{TOTAL} = the rms summation of the clock and ADC aperture jitter;

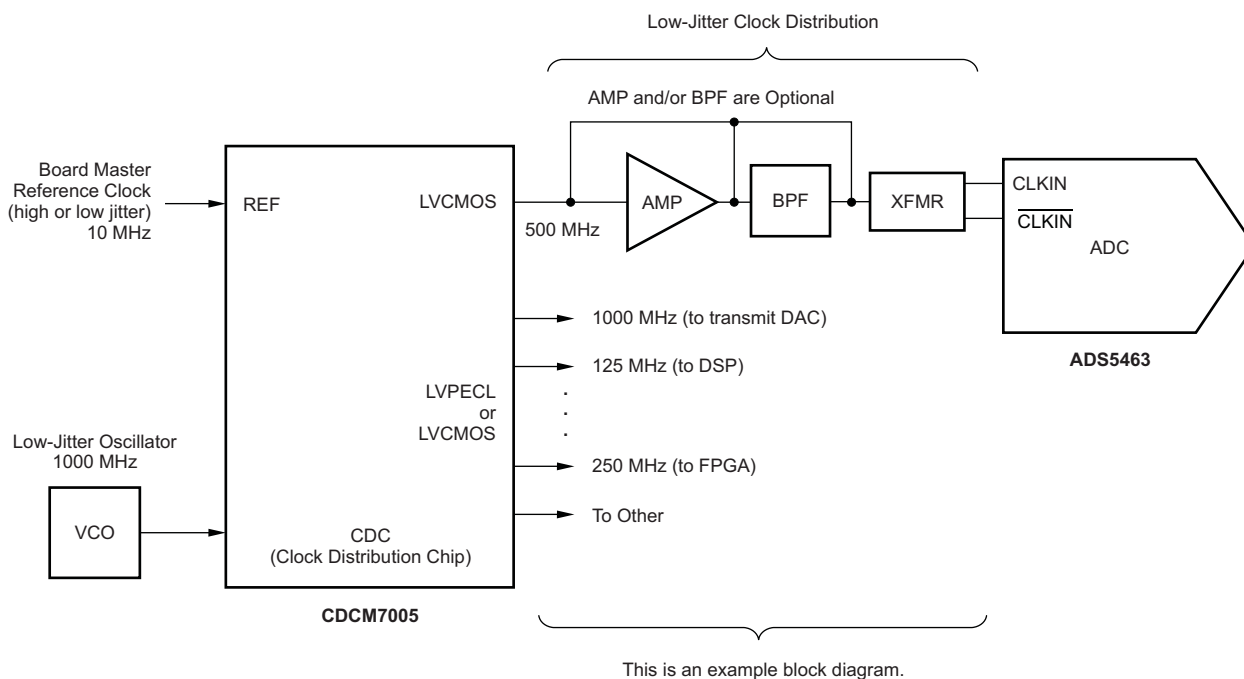
j_{ADC} = the ADC internal aperture jitter which is located in the data sheet;

j_{CLOCK} = the rms jitter of the clock at the clock input pins to the ADC; and

f_{IN} = the analog input frequency.

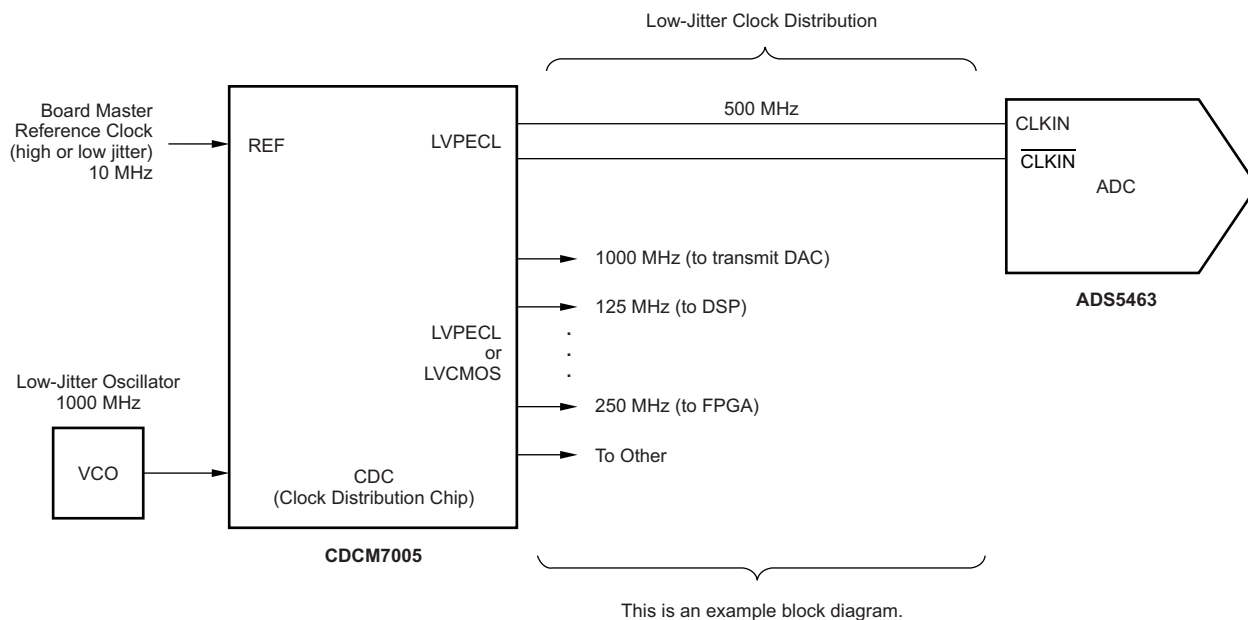
Notice that the SNR is a strong function of the analog input frequency, not the clock frequency. The slope of the clock source edges can have a mild impact on SNR as well and is not taken into account for these estimates. For this reason, maximizing clock source amplitudes at the ADC clock inputs is recommended, though not required (faster slope is desirable for jitter-related SNR). For more information on clocking high-speed ADCs, see Application Note [SLWA034](#), *Implementing a CDC7005 Low Jitter Clock Solution For High-Speed, High-IF ADC Devices*. Recommended clock distribution chips (CDCs) are the TI [CDC7005](#) and [CDCM7005](#). Depending on the jitter requirements, a band pass filter (BPF) is sometimes required between the CDC and the ADC. If the insertion loss of the BPF causes the clock amplitude to be too low for the ADC, or the clock source amplitude is too low to begin with, an inexpensive amplifier can be placed between the CDC and the BPF.

[Figure 46](#) represents a scenario where an LVCMOS single-ended clock output is used from a TI CDCM7005 with the clock signal path optimized for maximum amplitude and minimum jitter. This type of conditioning might generally be well-suited for use with greater than 250 MHz of input frequency. The jitter of this setup is difficult to estimate and requires a careful phase noise analysis of the clock path. The BPF (and possibly a low-cost amplifier because of insertion loss in the BPF) can improve the jitter between the CDC and ADC when the jitter provided by the CDC is still not adequate. The total jitter at the CDCM7005 output depends largely on the phase noise of the VCXO selected, as well as the CDCM7005, and typically has 50–100 fs of rms jitter. If it is determined that the jitter from the CDCM7005 with a VCXO is sufficient without further conditioning, it is possible to clock the ADS5463 directly from the CDCM7005 using differential LVPECL outputs, as illustrated in [Figure 47](#) (see the [CDCM7005 data sheet](#) for the exact schematic). This scenario may be more suitable for less than 150 MHz of input frequency where jitter is not as critical. A careful analysis of the required jitter and of the components involved is recommended before determining the proper approach.



Consult the [CDCM7005 data sheet](#) for proper schematic and specifications regarding allowable input and output frequency and amplitude ranges.

Figure 46. Optimum Jitter Clock Circuit



Consult the [CDCM7005 data sheet](#) for proper schematic and specifications regarding allowable input and output frequency and amplitude ranges.

Figure 47. Acceptable Jitter Clock Circuit

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Digital Outputs

The ADC provides 12 LVDS-compatible, offset binary data outputs (D11 to D0; D11 is the MSB and D0 is the LSB), a data-ready signal (DRY), and an over-range indicator (OVR). It is recommended to use the DRY signal to capture the output data of the ADS5463. DRY is source-synchronous to the DATA/OVR outputs and operates at the same frequency, creating a half-rate DDR interface that updates data on both the rising and falling edges of DRY. It is recommended that the capacitive loading on the digital outputs be minimized. Higher capacitance shortens the data-valid timing window. The values given for timing (see [Figure 1](#)) were obtained with a measured 10-pF parasitic board capacitance to ground on each LVDS line (or 5-pF differential parasitic capacitance). When setting the time relationship between DRY and DATA at the receiving device, it is generally recommended that setup time be maximized, but this partially depends on the setup and hold times of the device receiving the digital data (like an FPGA, Field Programmable Field Array). Since DRY and DATA are coincident, it will likely be necessary to delay either DRY or DATA such that setup time is maximized.

Referencing [Figure 1](#), the polarity of DRY with respect to the sample N data output transition is undetermined because of the unknown startup logic level of the clock divider that generates the DRY signal (DRY is a frequency divide-by-two of CLK). Either the rising or the falling edge of DRY will be coincident with sample N and the polarity of DRY could invert when power is cycled off/on. Data capture from the transition and not the polarity of DRY is recommended, but not required. If the synchronization of multiple ADS5463 devices is required, it might be necessary to use a form of the CLKIN signal rather than DRY to capture the data.

The DRY frequency is identical on the ADS5463 to the ADS5474 (where DRY equals 1/2 CLK frequency), but different than it is on the pin-similar ADS5444/ADS5440 (where DRY equals the CLK frequency). The LVDS outputs all require an external 100- Ω load between each output pair in order to meet the expected LVDS voltage levels. For long trace lengths, it may be necessary to place a 100- Ω load on each digital output as close to the ADS5474 as possible and another 100- Ω differential load at the end of the LVDS transmission line to provide matched impedance and avoid signal reflections. The effective load in this case reduces the LVDS voltage levels by half.

The OVR output equals a logic high when the 12-bit output word attempts to exceed either all 0s or all 1s. This flag is provided as an indicator that the analog input signal exceeded the full-scale input limit of approximately 2.2 V_{PP} (\pm gain error). The OVR indicator is provided for systems that use gain control to keep the analog input signal within acceptable limits.

Power Supplies

The ADS5463 uses three power supplies. For the analog portion of the design, a 5-V and 3.3-V supply (AVDD5 and AVDD3) are used, while the digital portion uses a 3.3-V supply (DVDD3). All of the ground pins are marked as GND, although analog and digital grounds are not tied together inside the package. The use of low-noise power supplies with adequate decoupling is recommended. Linear supplies are preferred to switched supplies; switched supplies tend to generate more noise components that can be coupled to the ADS5463. However, the PSRR value and the plot shown in Figure 48 were obtained without bulk supply decoupling capacitors. When bulk (0.1 μ F) decoupling capacitors are used, the board-level PSRR is much higher than the stated value for the ADC. The user may be able to supply power to the device with a less-than-ideal supply and still achieve good performance. It is not possible to make a single recommendation for every type of supply and level of decoupling for all systems. If the noise characteristics of the available supplies are understood, a study of the PSRR data for the ADS5463 may provide the user with enough information to select noisy supplies if the performance is still acceptable within the frequency range of interest. The power consumption of the ADS5463 does not change substantially over clock rate or input frequency as a result of the architecture and process. The DVDD3 PSRR is superior to both the AVDD5 and AVDD3 so was not graphed.

Because there are two diodes connected in reverse between AVDD3 and DVDD3 internally, a power-up sequence is recommended. When there is a delay in power up between these two supplies, the one that lags could have current sinking through an internal diode before it powers up. The sink current can be large or small depending on the impedance of the external supply and could damage the device or affect the supply source. The best power up sequence is one of the following options (regardless of when AVDD5 powers up):

- 1) Power up both AVDD3 and DVDD3 at the same time (best scenario), OR
- 2) Keep the voltage difference less than 0.8V between AVDD3 and DVDD3 during the power up (0.8V is not a hard specification - a smaller delta between supplies is safer).

If the above sequences are not practical then the sink current from the supply needs to be controlled or protection added externally. The max transient current (on the order of μ sec) for DVDD3 or AVDD3 pin is 500mA to avoid potential damage to the device or reduce its lifetime.

Values for analog and clock input given in the [Absolute Maximum Ratings](#) are valid when the supplies are on. When the power supplies are off and the clock or analog inputs are still alive, the input voltage and current needs to be limited to avoid device damage. If the ADC supplies are off, the max/min continuous DC voltage is ± 0.95 V and max DC current is 20 mA for each input pin (clock or analog), relative to ground.

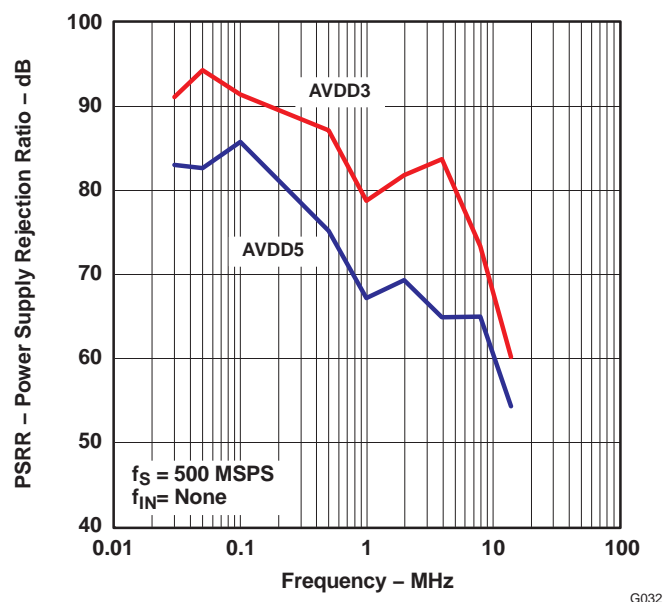


Figure 48. PSRR versus Supply Injected Frequency

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Operational Lifetime

It is important for applications that anticipate running continuously for long periods of time near the maximum-rated ambient temperature of +85°C to consider the data shown in [Figure 49](#) and [Figure 50](#). Referring to the [Thermal Characteristics](#) table, the worst-case operating condition with no airflow has a thermal rise of 23.7°C/W. At approximately 2.2 W of normal power dissipation, at a maximum ambient of +85°C with no airflow, the junction temperature of the ADS5463 reaches approximately $+85^{\circ}\text{C} + 23.7^{\circ}\text{C/W} \times 2.2\text{ W} = +137^{\circ}\text{C}$ and therefore the expected lifetime is approximately 8 years due to an electro migration failure and 18 years due to a wirebonding failure. Being even more conservative and accounting for the maximum possible power dissipation that is ensured (2.4 W), the junction temperature becomes nearly +142°C. As [Figure 49](#) and [Figure 50](#) show, this operating condition limits the expected lifetime of the ADS5463 even more. Operation at +85°C continuously may require airflow or an additional heatsink in order to decrease the internal junction temperature and increase the expected lifetime. An airflow of 250 LFM (linear feet per minute) reduces the thermal resistance to 16.4°C/W, the maximum junction temperature to +124°C and the expected lifetime to over 10 years, assuming a worst-case of 2.4 W and +85°C ambient. Of course, operation at lower ambient temperatures greatly increases the expected lifetime.

The ADS5463 performance over temperature is quite good and can be seen starting in [Figure 21](#). Though the typical plots show good performance at +100°C, the device is only rated from –40°C to +85°C. For continuous operation at temperatures near or above the maximum, aside from performance degradation, the expected primary negative effect is a shorter device lifetime.

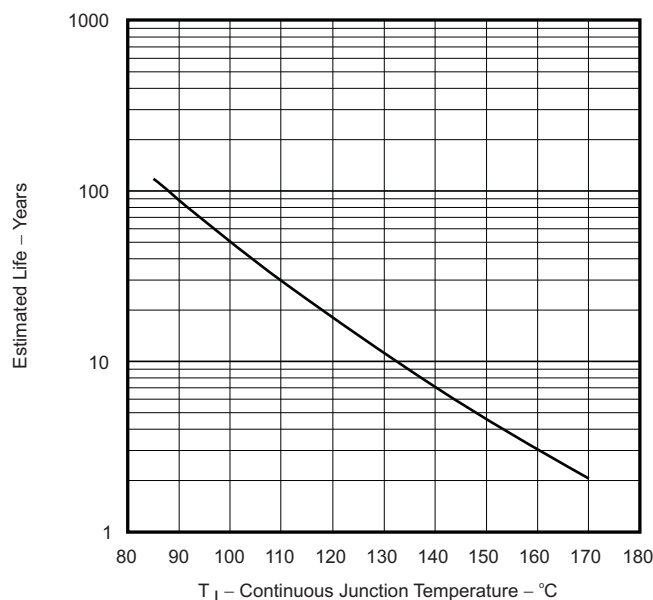


Figure 49. Operating Life Derating Chart, Electro Migration Fail Mode

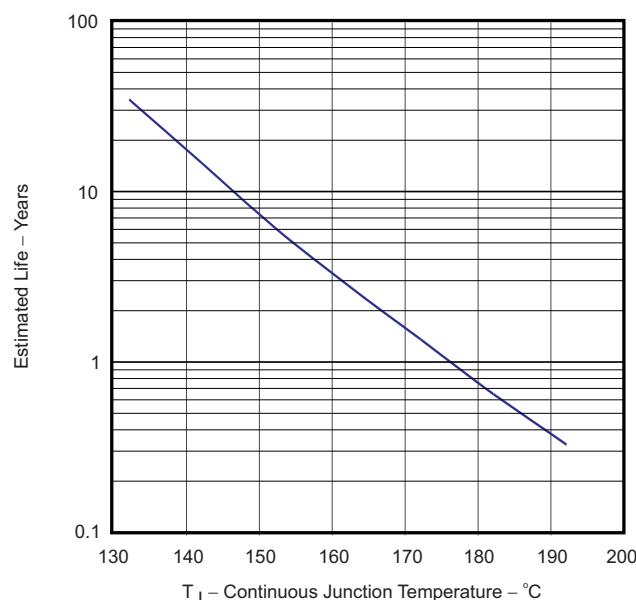


Figure 50. Operating Life Derating Chart, Wirebond Voiding Fail Mode

Layout Information

The evaluation board represents a good guideline of how to lay out the board to obtain the maximum performance from the ADS5463. General design rules, such as the use of multilayer boards, single ground plane for ADC ground connections, and local decoupling ceramic chip capacitors, should be applied. The input traces should be isolated from any external source of interference or noise, including the digital outputs as well as the clock traces. The clock signal traces should also be isolated from other signals, especially in applications where low jitter is required like high IF sampling. Besides performance-oriented rules, care must be taken when considering the heat dissipation of the device. The thermal heat sink should be soldered to the board as described in the [PowerPAD Package](#) section. See *ADS5463 EVM User Guide* ([SLAU194](#)) on the TI Web site for the evaluation board schematic.

PowerPAD Package

The PowerPAD package is a thermally enhanced standard-size IC package designed to eliminate the use of bulky heatsinks and slugs traditionally used in thermal packages. This package can be easily mounted using standard printed circuit board (PCB) assembly techniques, and can be removed and replaced using standard repair procedures.

The PowerPAD package is designed so that the leadframe die pad (or thermal pad) is exposed on the bottom of the IC. This provides an extremely low thermal resistance path between the die and the exterior of the package. The thermal pad on the bottom of the IC can then be soldered directly to the printed circuit board (PCB), using the PCB as a heatsink.

Assembly Process

1. Prepare the PCB top-side etch pattern including etch for the leads as well as the thermal pad as illustrated in the Mechanical Data section.
2. Place a 6-by-6 array of thermal vias in the thermal pad area. These holes should be 13 mils in diameter. The small size prevents wicking of the solder through the holes.
3. It is recommended to place a small number of 25-mil-diameter holes under the package, but outside the thermal pad area, to provide an additional heat path.
4. Connect all holes (both those inside and outside the thermal pad area) to an internal copper plane (such as a ground plane).
5. Do not use the typical web or spoke via-connection pattern when connecting the thermal vias to the ground plane. The spoke pattern increases the thermal resistance to the ground plane.
6. The top-side solder mask should leave exposed the terminals of the package and the thermal pad area.
7. Cover the entire bottom side of the PowerPAD vias to prevent solder wicking.
8. Apply solder paste to the exposed thermal pad area and all of the package terminals.

For more detailed information regarding the PowerPAD package and its thermal properties, see either the *PowerPAD Made Easy* application brief ([SLMA004](#)) or the *PowerPAD Thermally Enhanced Package* application report ([SLMA002](#)).

ADS5463

SLAS515B–NOVEMBER 2006–REVISED MAY 2008

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DEFINITION OF SPECIFICATIONS

Analog Bandwidth

The analog input frequency at which the power of the fundamental is reduced by 3 dB with respect to the low-frequency value

Aperture Delay

The delay in time between the rising edge of the input sampling clock and the actual time at which the sampling occurs

Aperture Uncertainty (Jitter)

The sample-to-sample variation in aperture delay

Clock Pulse Duration/Duty Cycle

The duty cycle of a clock signal is the ratio of the time the clock signal remains at a logic high (clock pulse duration) to the period of the clock signal, expressed as a percentage.

Differential Nonlinearity (DNL)

An ideal ADC exhibits code transitions at analog input values spaced exactly 1 LSB apart. DNL is the deviation of any single step from this ideal value, measured in units of LSB.

Common-Mode Rejection Ratio (CMRR)

CMRR measures the ability to reject signals that are presented to both analog inputs simultaneously. The injected common-mode frequency level is translated into dBFS, the spur in the output FFT is measured in dBFS, and the difference is the CMRR in dB.

Effective Number of Bits (ENOB)

ENOB is a measure in units of bits of a converter's performance as compared to the theoretical limit based on quantization noise

$$\text{ENOB} = (\text{SINAD} - 1.76)/6.02$$

Gain Error

Gain error is the deviation of the ADC actual input full-scale range from its ideal value, given as a percentage of the ideal input full-scale range.

Integral Nonlinearity (INL)

INL is the deviation of the ADC transfer function from a best-fit line determined by a least-squares curve fit of that transfer function. The INL at each analog input value is the difference between the actual transfer function and this best-fit line, measured in units of LSB.

Offset Error

Offset error is the deviation of output code from mid-code when both inputs are tied to common-mode.

Power-Supply Rejection Ratio (PSRR)

PSRR is a measure of the ability to reject frequencies present on the power supply. The injected frequency level is translated into dBFS, the spur in the output FFT is measured in dBFS, and the difference is the PSRR in dB. The measurement calibrates out the benefit of the board supply decoupling capacitors.

Signal-to-Noise Ratio (SNR)

SNR is the ratio of the power of the fundamental (P_S) to the noise floor power (P_N), excluding the power at dc and in the first five harmonics.

$$\text{SNR} = 10 \log_{10} \frac{P_S}{P_N} \quad (4)$$

SNR is either given in units of dBc (dB to carrier) when the absolute power of the fundamental is used as the reference, or dBFS (dB to full scale) when the power of the fundamental is extrapolated to the converter's full-scale range.

Signal-to-Noise and Distortion (SINAD)

SINAD is the ratio of the power of the fundamental (P_S) to the power of all the other spectral components including noise (P_N) and distortion (P_D), but excluding dc.

$$\text{SINAD} = 10 \log_{10} \frac{P_S}{P_N + P_D} \quad (5)$$

SINAD is either given in units of dBc (dB to carrier) when the absolute power of the fundamental is used as the reference, or dBFS (dB to full scale) when the power of the fundamental is extrapolated to the converter's full-scale range.

Temperature Drift

Temperature drift (with respect to gain error and offset error) specifies the change from the value at the nominal temperature to the value at T_{MIN} or T_{MAX} . It is computed as the maximum variation the parameters over the whole temperature range divided by $T_{\text{MIN}} - T_{\text{MAX}}$.

Total Harmonic Distortion (THD)

THD is the ratio of the power of the fundamental (P_S) to the power of the first five harmonics (P_D).

$$\text{THD} = 10 \log_{10} \frac{P_S}{P_D} \quad (6)$$

THD is typically given in units of dBc (dB to carrier).

Two-Tone Intermodulation Distortion (IMD3)

IMD3 is the ratio of the power of the fundamental (at frequencies f_1 , f_2) to the power of the worst spectral component at either frequency $2f_1 - f_2$ or $2f_2 - f_1$. IMD3 is given in units of either dBc (dB to carrier) when the absolute power of the fundamental is used as the reference, or dBFS (dB to full scale) when the power of the fundamental is extrapolated to the converter's full-scale range.

PACKAGING INFORMATION

Orderable Device	Status ⁽¹⁾	Package Type	Package Drawing	Pins	Package Qty	Eco Plan ⁽²⁾	Lead/Ball Finish	MSL Peak Temp ⁽³⁾
ADS5463IPFP	ACTIVE	HTQFP	PFP	80	96	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-4-260C-72 HR
ADS5463IPFPG4	ACTIVE	HTQFP	PFP	80	96	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-4-260C-72 HR
ADS5463IPFPR	ACTIVE	HTQFP	PFP	80	1000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-4-260C-72 HR
ADS5463IPFPRG4	ACTIVE	HTQFP	PFP	80	1000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-4-260C-72 HR

⁽¹⁾ The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

⁽²⁾ Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check <http://www.ti.com/productcontent> for the latest availability information and additional product content details.

TBD: The Pb-Free/Green conversion plan has not been defined.

Pb-Free (RoHS): TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

Pb-Free (RoHS Exempt): This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

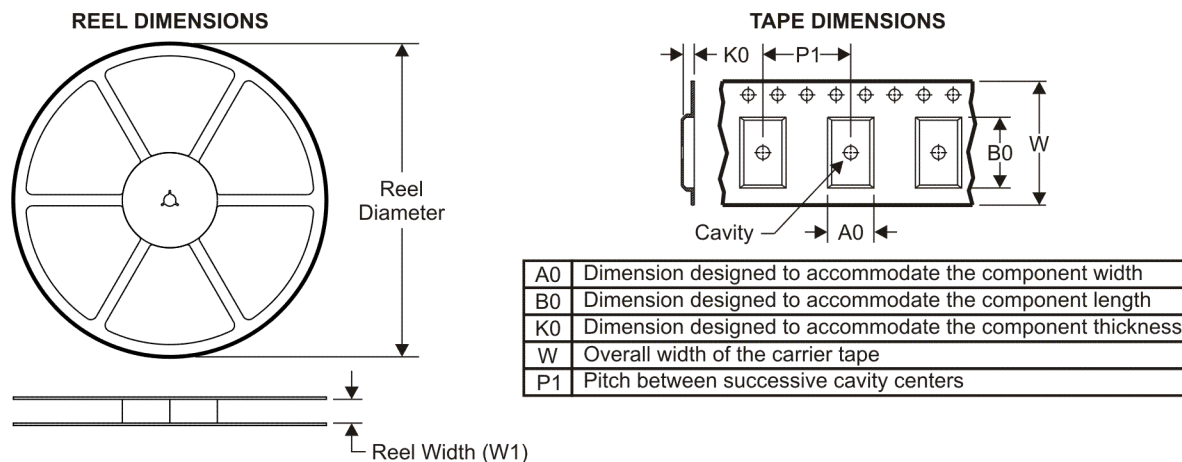
Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

⁽³⁾ MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

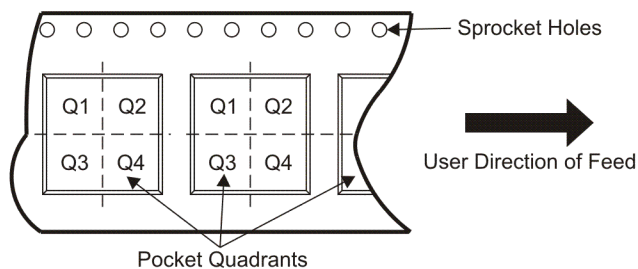
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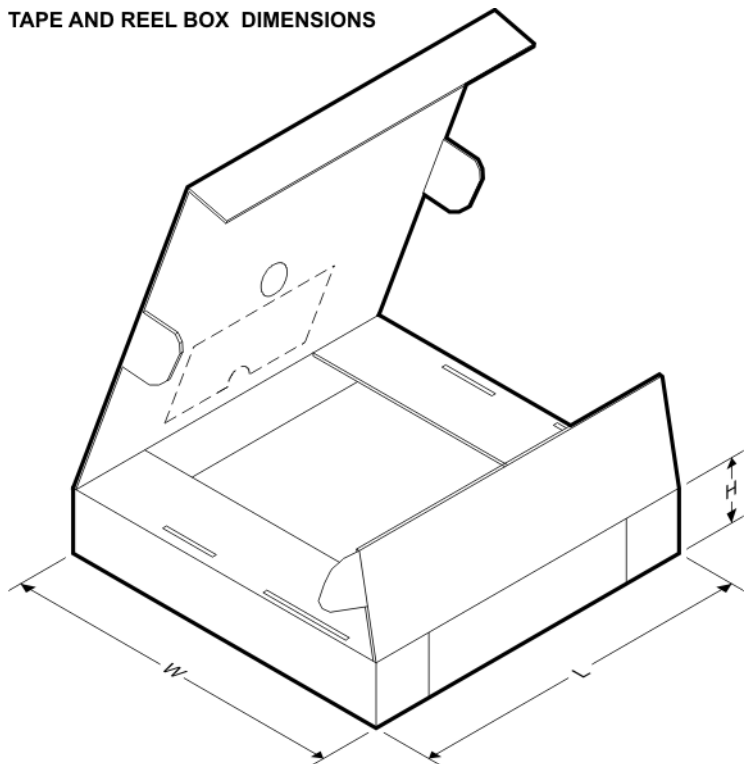
QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
ADS5463IPFPR	HTQFP	PFP	80	1000	330.0	24.4	15.0	15.0	1.5	20.0	24.0	Q2

TAPE AND REEL BOX DIMENSIONS



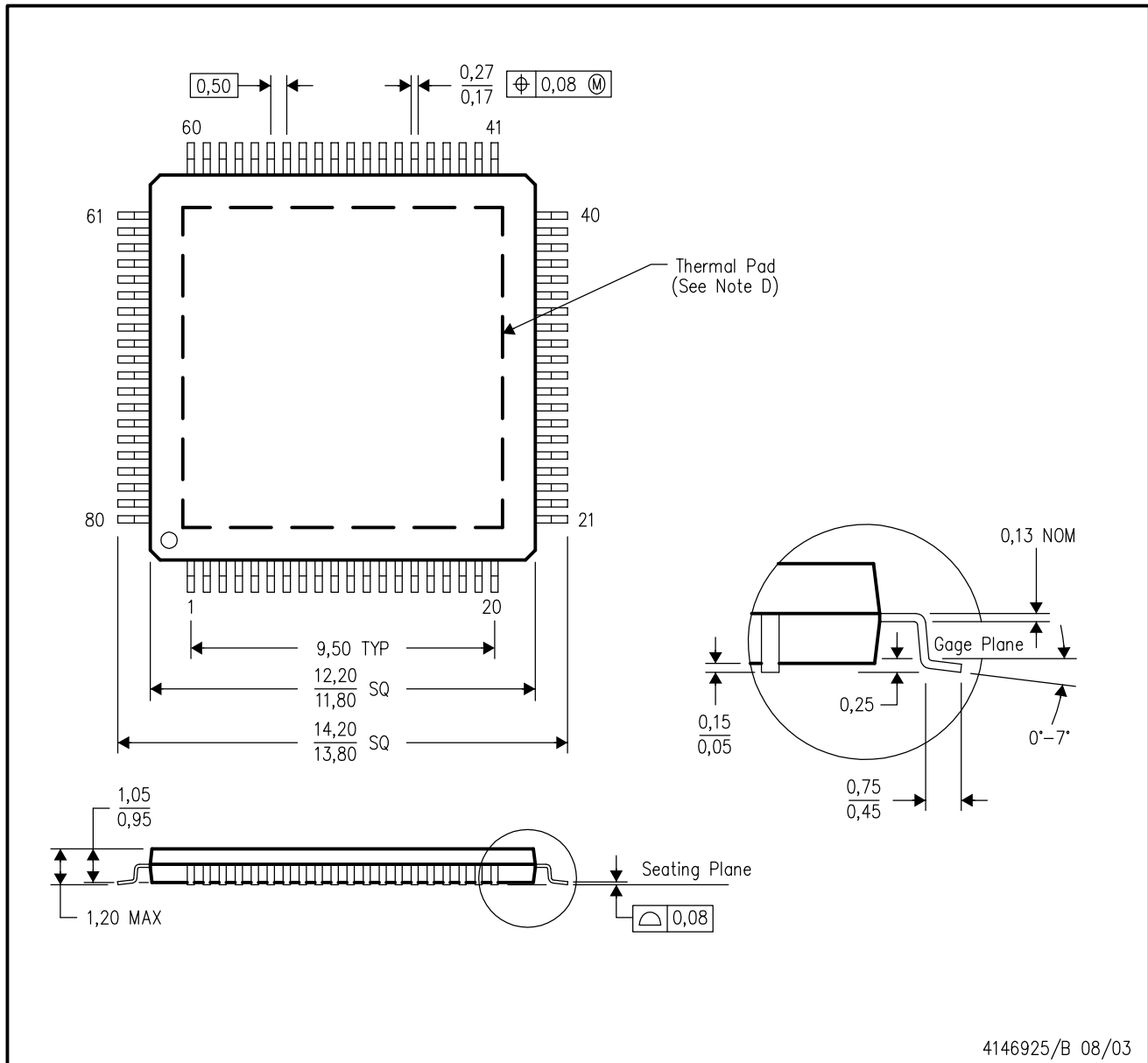
*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
ADS5463IPFPR	HTQFP	PFP	80	1000	333.2	345.9	31.8

MECHANICAL DATA

PFP (S-PQFP-G80)

PowerPAD™ PLASTIC QUAD FLATPACK



- NOTES:
- All linear dimensions are in millimeters.
 - This drawing is subject to change without notice.
 - Body dimensions do not include mold flash or protrusion
 - This package is designed to be soldered to a thermal pad on the board. Refer to Technical Brief, PowerPad Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 for information regarding recommended board layout. This document is available at www.ti.com <<http://www.ti.com>>.
 - Falls within JEDEC MS-026

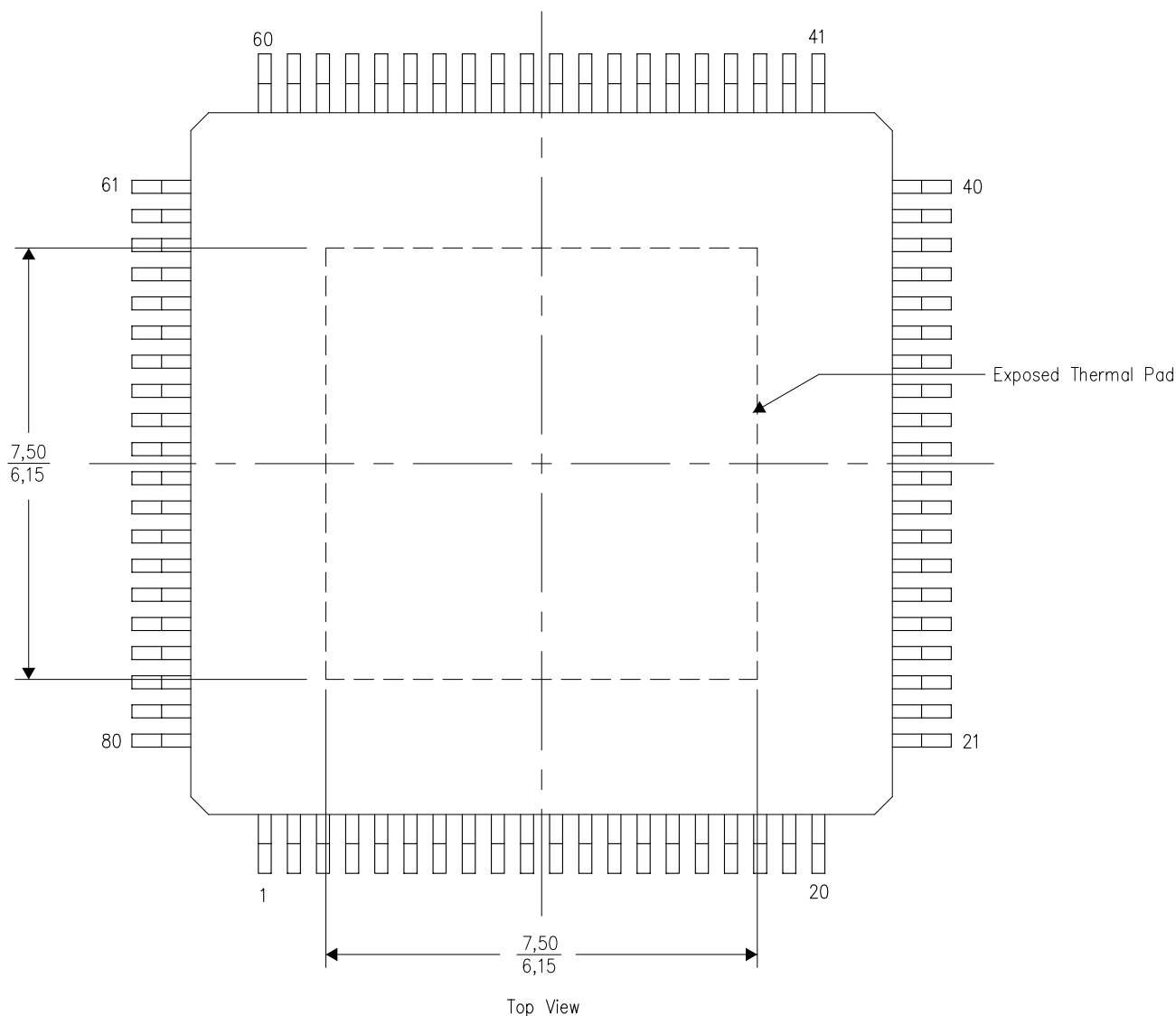
PowerPAD is a trademark of Texas Instruments.

THERMAL INFORMATION

This PowerPAD™ package incorporates an exposed thermal pad that is designed to be attached directly to an external heatsink. The thermal pad must be soldered directly to the printed circuit board (PCB). After soldering, the PCB can be used as a heatsink. In addition, through the use of thermal vias, the thermal pad can be attached directly to the appropriate copper plane shown in the electrical schematic for the device, or alternatively, can be attached to a special heatsink structure designed into the PCB. This design optimizes the heat transfer from the integrated circuit (IC).

For additional information on the PowerPAD package and how to take advantage of its heat dissipating abilities, refer to Technical Brief, PowerPAD Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 and Application Brief, PowerPAD Made Easy, Texas Instruments Literature No. SLMA004. Both documents are available at www.ti.com.

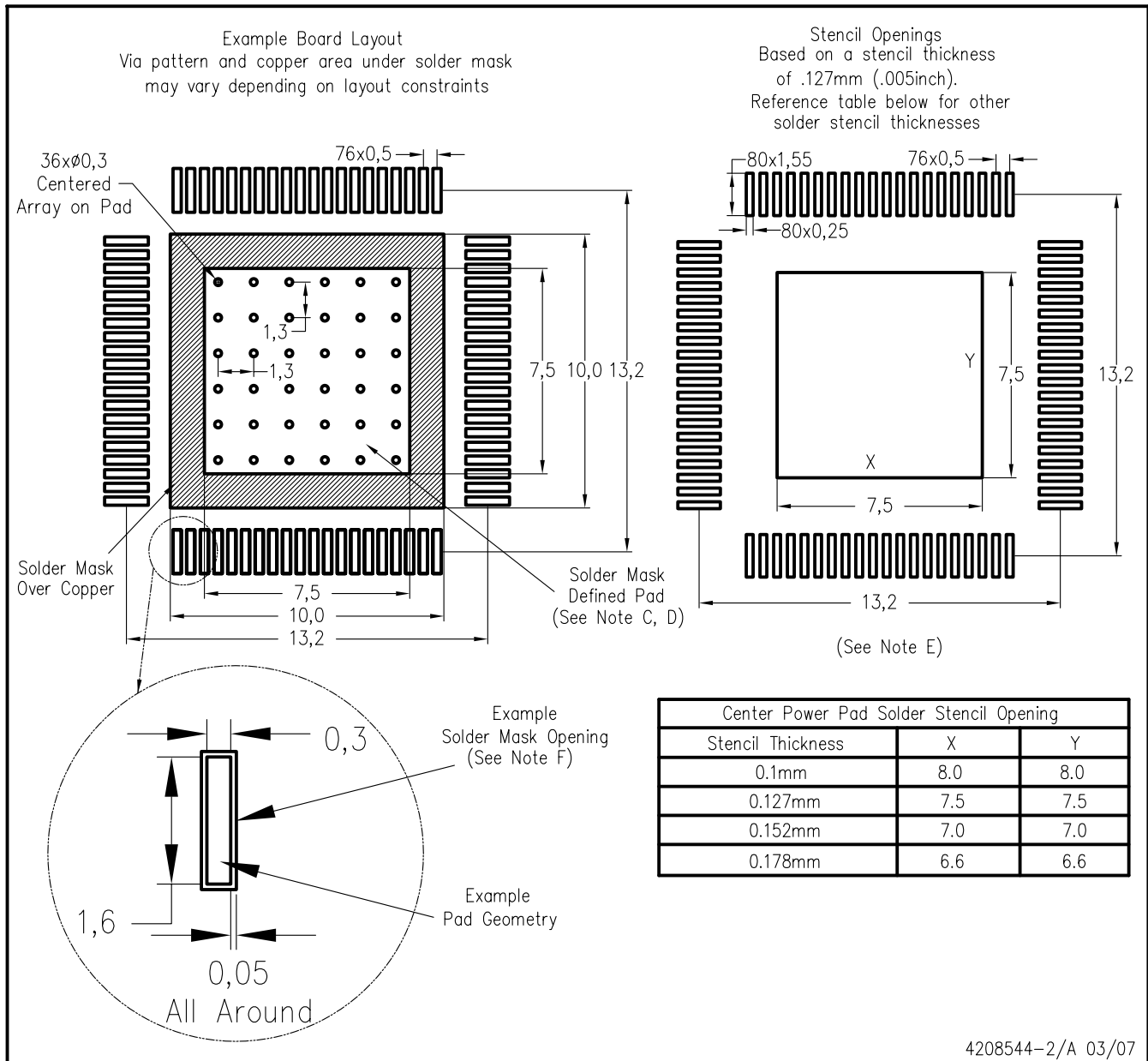
The exposed thermal pad dimensions for this package are shown in the following illustration.



NOTE: All linear dimensions are in millimeters

LAND PATTERN

PFP (S-PQFP-G80) PowerPAD™



4208544-2/A 03/07

- NOTES:
- All linear dimensions are in millimeters.
 - This drawing is subject to change without notice.
 - Customers should place a note on the circuit board fabrication drawing not to alter the center solder mask defined pad.
 - This package is designed to be soldered to a thermal pad on the board. Refer to Technical Brief, PowerPad Thermally Enhanced Package, Texas Instruments Literature No. SLMA002, SLMA004, and also the Product Data Sheets for specific thermal information, via requirements, and recommended board layout. These documents are available at www.ti.com <<http://www.ti.com>>. Publication IPC-7351 is recommended for alternate designs.
 - Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Example stencil design based on a 50% volumetric metal load solder paste. Refer to IPC-7525 for other stencil recommendations.
 - Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.

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