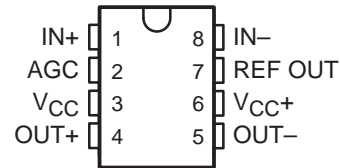


# TL026C DIFFERENTIAL HIGH-FREQUENCY AMPLIFIER WITH AGC

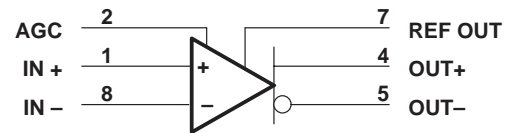
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- Low Output Common-Mode Sensitivity to AGC Voltages
- Input and Output Impedances Independent of AGC Voltage
- Peak Gain . . . 38 dB Typ
- Wide AGC Range . . . 50 dB Typ
- 3-dB Bandwidth . . . 50 MHz
- Other Characteristics Similar to NE592 and uA733

D OR P PACKAGE  
(TOP VIEW)



symbol



## description

This device is a monolithic two-stage high-frequency amplifier with differential inputs and outputs.

Internal feedback provides wide bandwidth, low phase distortion, and excellent gain stability. Variable gain based on signal summation provides large AGC control over a wide bandwidth with low harmonic distortion. Emitter-follower outputs enable the device to drive capacitive loads. All stages are current-source biased to obtain high common-mode and supply-voltage rejection ratios. The gain may be electronically attenuated by applying a control voltage to the AGC pin. No external compensation components are required.

This device is particularly useful in TV and radio IF and RF AGC circuits, as well as magnetic-tape and disk-file systems where AGC is needed. Other applications include video and pulse amplifiers where a large AGC range, wide bandwidth, low phase shift, and excellent gain stability are required.

The TL026C is characterized for operation from 0°C to 70°C.

## absolute maximum ratings over operating free-air temperature range (unless otherwise noted)†

Supply voltage, $V_{CC+}$ (see Note 1)	8 V
Supply voltage, $V_{CC-}$ (see Note 1)	– 8 V
Differential input voltage	±5 V
Common-mode input voltage	±6 V
Output current	±10 mA
Continuous total dissipation	See Dissipation Rating Table
Operating free-air temperature range	0°C to 70°C
Storage temperature range	– 65°C to 150°C
Lead temperature range 1,6 mm (1/16 inch) from case for 10 seconds	260°C

† Stresses beyond those listed under absolute maximum ratings may cause permanent damage to the device. This is a stress rating only, and functional operation of the device at these or any other conditions beyond those indicated in the recommended operating conditions section of this specification is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

NOTE 1: All voltages are with respect to the midpoint of  $V_{CC+}$  and  $V_{CC-}$  except differential input and output voltages.

DISSIPATION RATING TABLE

PACKAGE	$T_A \leq 25^\circ\text{C}$ POWER RATING	OPERATING FACTOR ABOVE $T_A = 25^\circ\text{C}$	$T_A = 70^\circ\text{C}$ POWER RATING
D	725 mW	5.8 mW/°C	464 mW
P	1000 mW	8.0 mW/°C	640 mW

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### recommended operating conditions

	MIN	NOM	MAX	UNIT
Supply voltage, $V_{CC+}$	3	6	8	V
Supply voltage, $V_{CC-}$	-3	-6	-8	V
Operating free-air temperature range, $T_A$	0		70	°C

### electrical characteristics at 25°C operating free-air temperature, $V_{CC+} = \pm 6$ V, $V_{AGC} = 0$ , REF OUT pin open (unless otherwise specified)

PARAMETER	FIGURE	TEST CONDITIONS	MIN	TYP	MAX	UNIT
$A_{VD}$ Large-signal differential voltage amplification	1	$V_{O(PP)} = 3$ V, $R_L = 2$ k $\Omega$	65	85	105	V/V
$\Delta A_{VD}$ Change in voltage amplification	1	$V_{IPP} = 28.5$ mV, $R_L = 2$ k $\Omega$ , $V_{AGC} - V_{ref} = \pm 180$ mV		-50		dB
$V_{ref}$ Voltage at REF OUT		$I_{ref} = -1$ mA to 100 $\mu$ A	1.3		1.5	V
BW Bandwidth (-3 dB)	2	$V_{O(PP)} = 1$ V, $V_{AGC} - V_{ref} = \pm 180$ mV		50		MHz
$I_{IO}$ Input offset current				0.4	5	$\mu$ A
$I_{IB}$ Input bias current				10	30	$\mu$ A
$V_{ICR}$ Common-mode input voltage range	3		$\pm 1$			V
$V_{OC}$ Common-mode output voltage	1	$R_L = \infty$	3.25	3.75	4.25	V
$\Delta V_{OC}$ Change in common-mode output voltage	1	$V_{AGC} = 0$ to 2 V, $R_L = \infty$			300	mV
$V_{OO}$ Output offset voltage	1	$V_{ID} = 0$ , $R_L = \infty$			0.75	V
$V_{O(PP)}$ Maximum peak-to-peak output voltage swing	1	$R_L = 2$ k $\Omega$	3	4		V
$r_i$ Input resistance at AGC, IN+, or IN-			10	30		k $\Omega$
$r_o$ Output resistance				20		$\Omega$
CMRR Common-mode rejection ratio	3	$V_{IC} = \pm 1$ V, $f = 100$ kHz	60	86		dB
		$V_{IC} = \pm 1$ V, $f = 5$ mHz		60		
$k_{SVR}$ Supply voltage rejection ratio ( $\Delta V_{CC+} / \Delta V_{IO}$ )	4	$\Delta V_{CC+} = \pm 0.5$ V, $\Delta V_{CC-} = \pm 0.5$ V	50	70		dB
$V_n$ Broadband equivalent noise voltage	4	BW = 1 kHz to 10 MHz		12		$\mu$ V
$t_{pd}$ Propagation delay time	2	$\Delta V_O = 1$ V		6	10	ns
$t_r$ Rise time	2	$\Delta V_O = 1$ V		4.5	12	ns
$I_{sink(max)}$ Maximum output sink current		$V_{ID} = 1$ V, $V_O = 3$ V	3	4		mA
$I_{CC}$ Supply current		No load, No signal		22	27	mA

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electrical characteristics over recommended operating free-air temperature range,  $V_{CC\pm} = \pm 6\text{ V}$ ,  $V_{AGC} = 0$ , REF OUT pin open (unless otherwise specified)

PARAMETER	FIGURE	TEST CONDITIONS	MIN	TYP	MAX	UNIT
$A_{VD}$ Large-signal differential voltage amplification	1	$V_{O(PP)} = 3\text{ V}$ , $R_L = 2\text{ k}\Omega$	55		115	V/V
$I_{IO}$ Input offset current					6	$\mu\text{A}$
$I_{IB}$ Input bias current					40	$\mu\text{A}$
$V_{ICR}$ Common-mode input voltage range	3		$\pm 1$			V
$V_{OO}$ Output offset voltage	1	$V_{ID} = 0$ , $R_L = \infty$			1.5	V
$V_{O(PP)}$ Maximum peak-to-peak output voltage swing	1	$R_L = 2\text{ k}\Omega$	2.8			V
$r_i$ Input resistance at AGC, IN+, or IN –			8			$\text{k}\Omega$
CMRR Common-mode rejection ratio	3	$V_{IC} = \pm 1\text{ V}$ , $f = 100\text{ kHz}$	50			dB
$k_{SVR}$ Supply voltage rejection ratio ( $\Delta V_{CC} / \Delta V_{IO}$ )	4	$\Delta V_{CC+} = \pm 0.5\text{ V}$ , $\Delta V_{CC-} = \pm 0.5\text{ V}$	50			dB
$I_{\text{sink(max)}}$ Maximum output sink current		$V_{ID} = 1\text{ V}$ , $V_O = 3\text{ V}$	2.8	4		mA
$I_{CC}$ Supply current	1	No load, No signal			30	mA

### PARAMETER MEASUREMENT INFORMATION

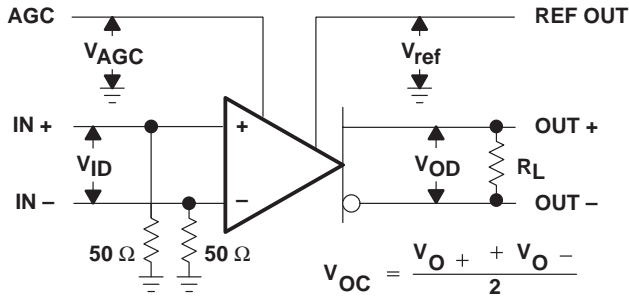


Figure 1. Test Circuit

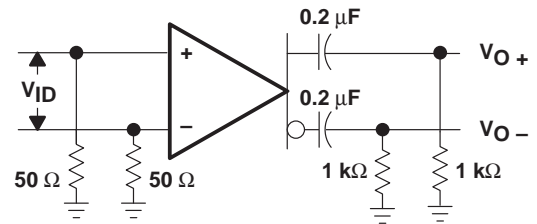


Figure 2. Test Circuit

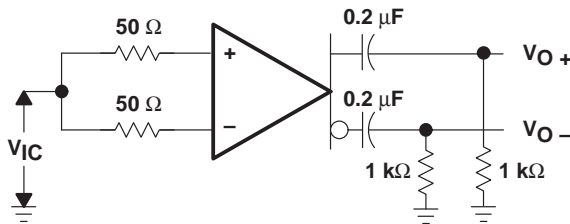


Figure 3. Test Circuit

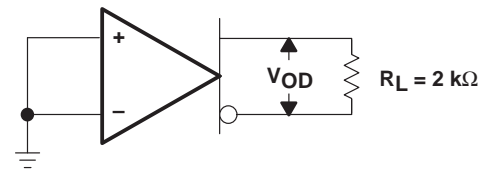


Figure 4. Test Circuit

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## DIFFERENTIAL HIGH-FREQUENCY AMPLIFIER WITH AGC

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### TYPICAL CHARACTERISTICS

DIFFERENTIAL VOLTAGE AMPLIFICATION  
vs  
DIFFERENTIAL GAIN-CONTROL VOLTAGE

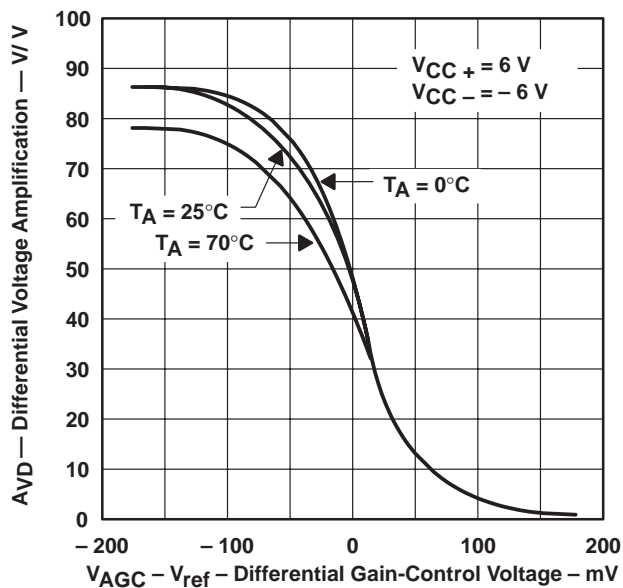


Figure 5

## APPLICATION INFORMATION

### gain characteristics

Figure 5 shows the differential voltage amplification versus the differential gain-control voltage ( $V_{AGC} - V_{ref}$ ).  $V_{AGC}$  is the absolute voltage applied to the  $A_{GC}$  input and  $V_{ref}$  is the dc voltage at the REF OUT output. As  $V_{AGC}$  increases with respect to  $V_{ref}$ , the TL026C gain changes from maximum to minimum. As shown in Figure 5 for example,  $V_{AGC}$  would have to vary from approximately 180 mV less than  $V_{ref}$  to approximately 180 mV greater than  $V_{ref}$  to change the gain from maximum to minimum. The total signal change in  $V_{AGC}$  is defined by the following equation.

$$\begin{aligned}\Delta V_{AGC} &= V_{ref} + 180 \text{ mV} - (V_{ref} - 180 \text{ mV}) \\ \Delta V_{AGC} &= 360 \text{ mV}\end{aligned}\tag{1}$$

However, because  $V_{AGC}$  varies as the ac AGC signal varies and also differentially around  $V_{ref}$ , then  $V_{AGC}$  should have an ac signal component and a dc component. To preserve the dc and thermal tracking of the device, this dc voltage must be generated from  $V_{ref}$ . To apply proper bias to the AGC input, the external circuit used to generate  $V_{AGC}$  must combine these two voltages. Figures 6 and 7 show two circuits that will perform this operation and are easy to implement. The circuits use a standard dual operational amplifier for AGC feedback. By providing rectification and the required feedback gain, these circuits are also complete AGC systems.

### circuit operation

Amplifier A1 amplifies and inverts the rectified and filtered AGC signal voltage  $V_C$  producing output voltage  $V_1$ . Amplifier A2 is a differential amplifier that inverts  $V_1$  again and adds the scaled  $V_{ref}$  voltage. This conditioning makes  $V_{AGC}$  the sum of the signal plus the scaled  $V_{ref}$ . As the signal voltage increases,  $V_{AGC}$  increases and the gain of the TL026C is reduced. This maintains a constant output level.

### feedback circuit equations

Following the AGC input signal (Figures 6 and 7) from the OUT output through the feedback amplifiers to the AGC input produces the following equations:

1. AC output to diode D1, assuming sinusoidal signals
 
$$V_O = V_{OP} (\sin wt)\tag{2}$$

where:

$$V_{OP} = \text{peak voltage of } V_O$$

2. Diode D1 and capacitor C1 output
 
$$V_C = V_{OP} - V_F\tag{3}$$

where:

$$V_F = \text{forward voltage drop of D1}$$

$$V_C = \text{voltage across capacitor C1}$$

3. A1 output
 
$$V_1 = -\frac{R_2}{R_1} V_C\tag{4}$$

4. A2 output ( $R_3 = R_4$ )
 
$$V_{AGC} = \frac{R_2}{R_1} V_C + 2\frac{R_6}{R_5 + R_6} V_{ref}\tag{5}$$

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### APPLICATION INFORMATION

Amplifier A2 inverts V1 producing a positive AGC signal voltage. Therefore, the input voltage to the TL026C AGC pin consists of an AGC signal equal to:

$$\frac{R2}{R1} V_C \quad (6)$$

and a dc voltage derived from  $V_{ref}$ , defined as the quiescent value of  $V_{AGC}$ .

$$V_{AGC}(q) = 2 \frac{R6}{R5 + R6} V_{ref} \quad (7)$$

For the initial resistor calculations,  $V_{ref}$  is assumed to be typically 1.4 V making quiescent  $V_{AGC}$  approximately 1.22 V ( $V_{AGC}(q) = V_{ref} - 180 \text{ mV}$ ). This voltage allows the TL026C to operate at maximum gain under no-signal and low-signal conditions. In addition, with  $V_{ref}$  used as both internal and external reference, its variation from device to device automatically adjusts the overall bias and makes AGC operation essentially independent of the absolute value of  $V_{ref}$ . The resistor divider needs to be calculated only once and is valid for the full tolerance of  $V_{ref}$ .

### output voltage limits (see Figures 6 and 7)

The output voltage level desired must fall within the following limits:

1. Because the data sheet minimum output swing is 3 V peak-to-peak using a 2-k $\Omega$  load resistor, the user-selected design limit for the peak output swing should not exceed 1.5 V.
2. The voltage drop of the rectifying diode determines the lower voltage limit. When a silicon diode is used, this voltage is approximately 0.7 V. The output voltage  $V_O$  must have sufficient amplitude to exceed the rectifying diode drop. A Schottky diode can be used to reduce the  $V_O$  level required.

### gain calculations for a peak output voltage of 1 V

A peak output voltage of 1 V was chosen for gain calculations because it is approximately midway between the limits of conditions 1 and 2 in the preceding paragraph.

Using equation 3 ( $V_C = V_{OP} - V_d$ ),  $V_C$  is calculated as follows:

$$V_C = 1 \text{ V} - 0.7 \text{ V}$$

$$V_C = 0.3 \text{ V}$$

Therefore, the gain of A1 must produce a voltage V1 that is equal to or greater than the total change in  $V_{AGC}$  for maximum TL026C gain change.

With a total change in  $V_{AGC}$  of 360 mV and using equation 4, the calculation is as follows:

$$-\frac{V1}{V_C} = \frac{\Delta V_{AGC}}{V_C} = \frac{R2}{R1} = \frac{0.36}{0.3} = 1.2$$

If R1 is 10 k $\Omega$ , R2 is 1.2 times R1 or 12 k $\Omega$ .

Since the output voltage for this circuit must be between 0.85 V and 1.3 V, the component values in Figures 6 and 7 provide a nominal 1-V peak output limit. This limit is the best choice to allow for temperature variations of the diode and minimum output voltage specification.

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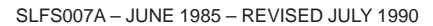
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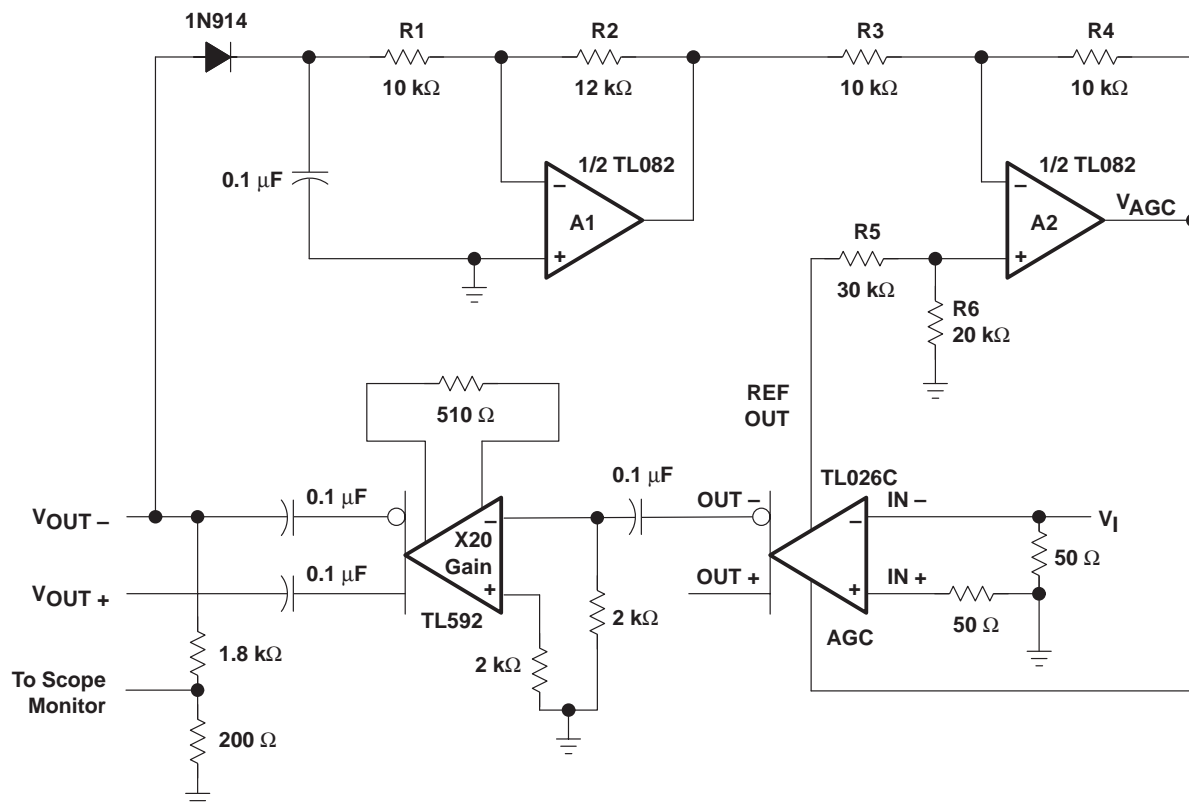
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### APPLICATION INFORMATION



NOTE:  $V_{CC+} = +6$  V and  $V_{CC-} = -6$  V for TL026C and amplifiers A1 and A2.

**Figure 7. Typical Application Circuit With Attenuation**



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