

Stereo 2.6W Audio Power Amplifier (With DC\_Volume Control)

#### **Features**

- Low Operating Current with 9mA
- Improved Depop Circuitry to Eliminate Turn-on and Turn-off Transients in Outputs
- High PSRR
- 32 Steps Volume Adjustable by DC Voltage with Hysteresis
- 2.6W per Channel Output Power into 4W Load at 5V, BTL Mode
- Two Output Modes Allowable with BTL and SE Modes Selected by SE/BTL pin
- Low Current Consumption in Shutdown Mode (1mA)
- Short-Circuit Protection
- Thermal Shutdown Protection and Over-Current Protection Circuitry
- Maximum Output Swing Clamping Function
- · The OUT+ Signal and the IN- Signal are Outphase
- SOP-16P Packages with Thermal Pad Package
- Lead Free and Green Devices Available (RoHS Compliant)

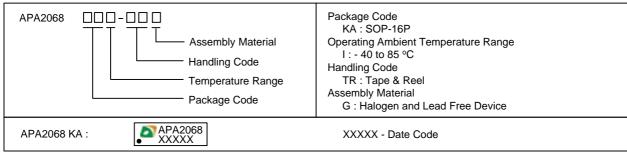
## **General Description**

APA2068 is a monolithic integrated circuit, which provides precise DC volume control, and a stereo bridged audio power amplifiers capable of producing 2.6W (1.8W) into  $4\Omega$  with less than 10% (1.0%) THD+N. The attenuator range of the volume control in APA2068 is from 20dB (DC\_Vol=0V) to -80dB (DC\_Vol=3.54V) with 32 steps. The advantage of internal gain setting can be less components and PCB area. Both of the depop circuitry and the thermal shutdown protection circuitry are integrated in APA2068, that reduce pops and clicks noise during power up or shutdown mode operation. It also improves the power off pop noise and protects the chip from being destroyed by over temperature and short current failure. To simplify the audio system design, APA2068 combines a stereo bridge-tied loads (BTL) mode for speaker drive and a stereo single-end (SE) mode for headphone drive into a single chip, where both modes are easily switched by the SE/BTL input control pin signal.

## **Applications**

- NBs
- LCD Monitor or TVs

# Ordering and Marking Information

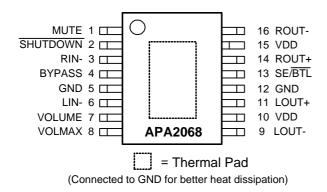


Note: ANPEC lead-free products contain molding compounds/die attach materials and 100% matte tin plate termination finish; which are fully compliant with RoHS. ANPEC lead-free products meet or exceed the lead-free requirements of IPC/JEDEC J-STD-020C for MSL classification at lead-free peak reflow temperature. ANPEC defines "Green" to mean lead-free (RoHS compliant) and halogen free (Br or Cl does not exceed 900ppm by weight in homogeneous material and total of Br and Cl does not exceed 1500ppm by weight).

ANPEC reserves the right to make changes to improve reliability or manufacturability without notice, and advise customers to obtain the latest version of relevant information to verify before placing orders.



# **Pin Configuration**



## **Absolute Maximum Ratings**

(Over operating free-air temperature range unless otherwise noted.)

Symbol	Parameter	Rating	Unit
V <sub>DD</sub>	Supply Voltage Range	-0.3 to 6	V
V <sub>IN</sub>	Input Voltage Range, SE/BTL, SHUTDOWN, MUTE	-0.3 to V <sub>DD</sub> +0.3	V
TJ	Maximum Junction Temperature	150	°C
T <sub>STG</sub>	Storage Temperature Range	-65 to +150	°C
T <sub>SDR</sub>	Maximum Lead Soldering Temperature,10 Seconds	260	°C
P <sub>D</sub>	Power Dissipation	Internal Limited	W

## **Thermal Characteristics**

Symbol	Parameter	Typical Value	Unit
θда	Thermal Resistance from Junction to Ambient in Free Air  SOP-16P	45	°C/W

## **Recommended Operating Conditions**

Symbol	Parameter			Range		
Symbol	Farameter	Min.	Max.	Unit		
V <sub>DD</sub>	Supply Voltage	4.5	5.5	V		
T <sub>A</sub>	Operating Ambient Temperature Range	-40	85	°C		
TJ	Operating Junction Temperature	-	125	°C		
V <sub>IH</sub>	High Level Threshold Voltage	SHUTDOWN, MUTE	2	-	V	
VIH	I light Level Threshold Voltage	SE/BTL	4	-	V	
V <sub>IL</sub>	Low Level Threshold Voltage	SHUTDOWN, MUTE	-	1.0	V	
VIL	SE/BTL		-	1	V	
V <sub>ICM</sub>	Common Mode Input Voltage		V <sub>DD</sub> -1.0	-	V	



## **Electrical Characteristics**

 $V_{DD} = 5V$ ,  $T_A = 25$ °C (unless otherwise noted)

Symbol	Parameter	Test Conditions		Unit		
Syllibol	Farameter	rest conditions	Min.	Min. Typ. Max.	Unit	
	Supply Current	SE/BTL=0V	1	9	20	m ^
IDD	I <sub>DD</sub> Supply Current	SE/BTL=5V	-	4	10	mA
	Supply Current in Shutdown Mode	SE/BTL=0V		1 -		
I <sub>SD</sub>		SHUTDOWN=0V	-		μΑ	
I <sub>IH</sub>	High Input Current		-	900	-	nA
I <sub>IL</sub>	Low Input Current		-	900	-	nA
Vos	Output Differential Voltage		-	5	-	mV

Operating Characteristics, BTL mode

 $V_{DD}$  = 5V,  $T_A$  = 25°C,  $R_L$  = 4 $\Omega$ , Gain = 2V/V (unless otherwise noted)

Symbol	Parameter	Test Conditions	APA2068			Unit	
	Parameter	rest Conditions	Min.	Тур.	Max.	Onit	
		THD+N=10%, $R_L=3\Omega$ , $f_{in}=1kHz$	-	2.9	-		
		THD+N=10%, $R_L=4\Omega$ , $f_{in}=1kHz$	-	2.6	-		
Po	Maximum Output Power	THD+N=10%, R <sub>L</sub> =8 $\Omega$ , f <sub>in</sub> = 1kHz	-	1.6	-	W	
F0	Maximum Output Fower	THD+N=1%, $R_L=3\Omega$ , $f_{in}=1kHz$	-	2.4	-		
		THD+N=1%, $R_L=4\Omega$ , $f_{in}=1kHz$	-	1.8	-		
		THD+N=1%, $R_L=8\Omega$ , $f_{in}=1kHz$	1	1.3	-		
THD+N	Total Harmonia Distortion Diva Naisa	$P_O = 1.2W$ , $R_L = 4\Omega$ , $f_{in} = 1kHz$	-	0.07	-	%	
I HD+N	Total Harmonic Distortion Plus Noise			0.08	-	,3	
PSRR	Power Ripple Rejection Ratio	$V_{rr}$ = 0.1 $V$ rms, $R_L$ = $8\Omega$ , $C_B$ = $1\mu$ F, $f_{in}$ = $120$ Hz	-	60	-	dB	
Crosstalk	Channel Separation	$C_B = 1\mu F$ , $R_L = 8\Omega$ , $f_{in} = 1kHz$	-	90	-	dB	
S/N	Signal to Noise Ratio	$P_0 = 1.1W$ , $R_L = 8\Omega$ , A_Weighting	-	95	-	dB	

Operating Characteristics, SE mode.  $V_{DD} = 5V$ ,  $T_A = 25$  °C, Gain = 1V/V (unless otherwise noted)

Cumbal	B	Test Conditions		I I m i t			
Symbol	Parameter	Test Conditions	Min.	Тур.		Unit	
		THD+N= 10%, $R_L = 16\Omega$ , $f_{in} = 1kHz$	-	220	-		
В	Maximum Output Power	THD+N= 10%, $R_L$ = 32 $\Omega$ , $f_{in}$ = 1kHz	-	120	-	mW	
P <sub>o</sub> M	Maximum Output Power	THD+N = 1%, $R_L$ = 16 $\Omega$ , $f_{in}$ = 1kHz	-	160	-	IIIVV	
		THD+N = 1%, $R_L$ = 32 $\Omega$ , $f_{in}$ = 1kHz	-	95	-		
THD+N	$P_0 = 125$ mW, $R_L = 16\Omega$ , $f_{in} = 1$ kHz		-	0.09	-	%	
I ND+N	Total Harmonic Distortion Plus Noise	$P_0 = 65$ mW, $R_L = 32\Omega$ , $f_{in} = 1$ kHz	-	0.09	-	70	
PSRR	Power Ripple Rejection Ratio	$V_{IN}$ = 0.1Vrms, $R_L$ = $8\Omega$ , $C_B$ = $1\mu F$ , $f_{in}$ = 120Hz	-	60	-	dB	
Crosstalk	Channel Separation	$C_B = 1\mu F$ , $R_L = 32\Omega$ , $f_{in} = 1kHz$	-	60	-	dB	
S/N	Signal to Noise Ratio	$P_0 = 75$ mW, SE, $R_L = 32\Omega$ , A_Weighting	-	100	-	dB	



# **Pin Description**

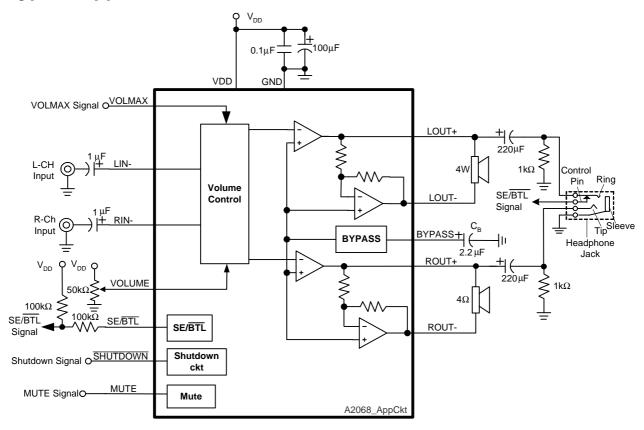
F	PIN		FUNCTION			
NO.	NAME	I/O	FUNCTION			
1	MUTE	1	Mute control signal input, hold low for normal operation, hold high to mute.			
2	SHUTDOWN	I	It will be into shutdown mode when pull low. $I_{SD} = 1\mu A$			
3	RIN-	I	Right channel input terminal			
4	BYPASS	I	Bias voltage generator			
5,12	GND	-	Ground connection, Connected to thermal pad.			
6	LIN-	I	Left channel input terminal			
7	VOLUME	I	Input signal for internal volume gain setting.			
8	VOLMAX	I	Setting the maximum output swing. Input a non-zero voltage ( $V_C$ ) to this pin, the output voltage swing will be clamped between $V_{OH}$ (the maximum positive value) - $V_C \& V_{OL}$ (the minimum negative value) + $V_C$ . Disable this function when tie this pin to GND. Maximum input voltage $\leq$ 1/2 $V_{DD}$ .			
9	LOUT-	0	Left channel negative output in BTL mode and high impedance in SE mode.			
10,15	VDD	-	Supply voltage			
11	LOUT+	0	Left channel positive output in BTL mode and SE mode.			
13	SE/BTL	I	Output mode control input, high for SE output mode and low for BTL mode.			
14	ROUT+	0	Right channel positive output in BTL mode and SE mode.			
16	ROUT-	0	Right channel negative output in BTL mode and high impedance in SE mode.			

# **Control Input Table**

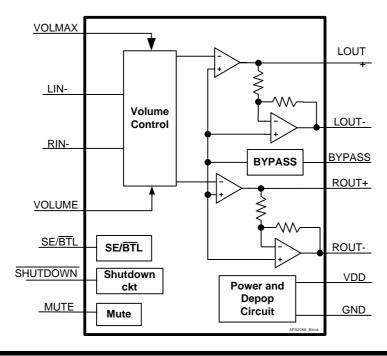
SHUTDOWN	MUTE	SE/BTL	Operating Mode
L	X	X	Shutdown mode
Н	L	L	BTL out
Н	L	Н	SE out
Н	Н	X	Mute



# **Typical Application Circuit**



## **Block Diagram**





# Volume Control Table\_BTL Mode

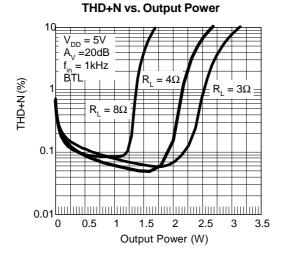
Supply Voltage  $V_{\rm DD} = 5V$ 

Gain (dB)	High (V)	Low (V)	Hysteresis (mV)	Recommended Voltage (V)
20	0.12	0.00		0
18	0.23	0.17	52	0.20
16	0.34	0.28	51	0.31
14	0.46	0.39	50	0.43
12	0.57	0.51	49	0.54
10	0.69	0.62	47	0.65
8	0.80	0.73	46	0.77
6	0.91	0.84	45	0.88
4	1.03	0.96	44	0.99
2	1.14	1.07	43	1.10
0	1.25	1.18	41	1.22
-2	1.37	1.29	40	1.33
-4	1.48	1.41	39	1.44
-6	1.59	1.52	38	1.56
-8	1.71	1.63	37	1.67
-10	1.82	1.74	35	1.78
-12	1.93	1.85	34	1.89
-14	2.05	1.97	33	2.01
-16	2.16	2.08	32	2.12
-18	2.28	2.19	30	2.23
-20	2.39	2.30	29	2.35
-22	2.50	2.42	28	2.46
-24	2.62	2.53	27	2.57
-26	2.73	2.64	26	2.69
-28	2.84	2.75	24	2.80
-30	2.96	2.87	23	2.91
-32	3.07	2.98	22	3.02
-34	3.18	3.09	21	3.14
-36	3.30	3.20	20	3.25
-38	3.41	3.32	18	3.36
-40	3.52	3.43	17	3.48
-80	5.00	3.54	16	5
	1	1	i .	

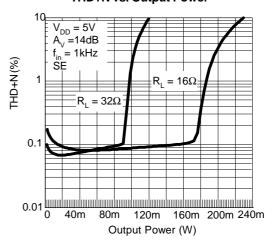


# **Typical Operating Characteristics**

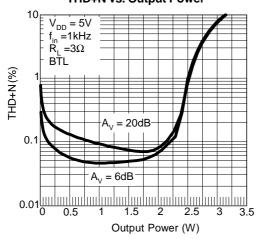


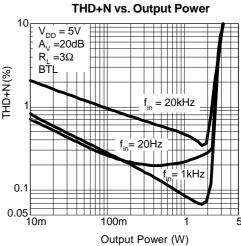


### THD+N vs. Output Power

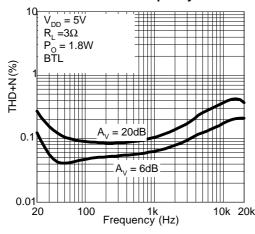


### THD+N vs. Output Power

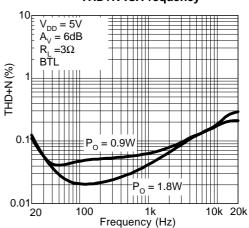




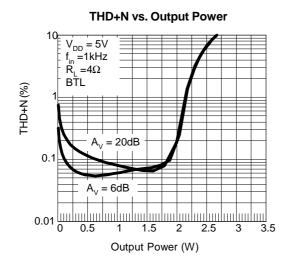
### THD+N vs. Frequency

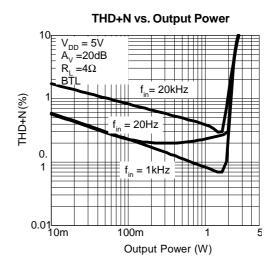


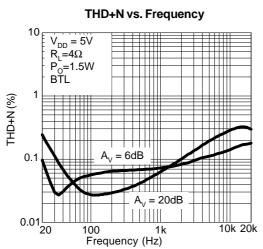
THD+N vs. Frequency

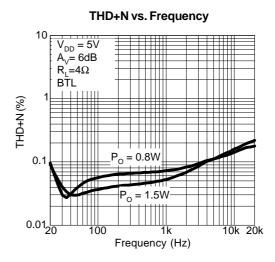


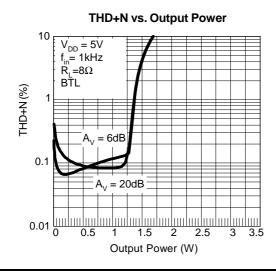


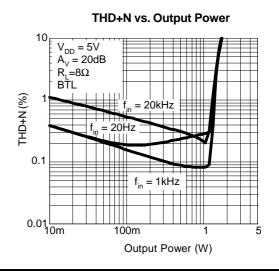




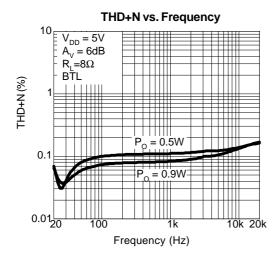


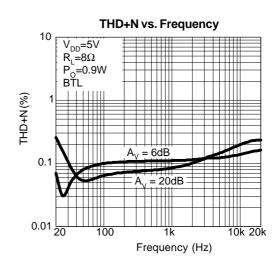


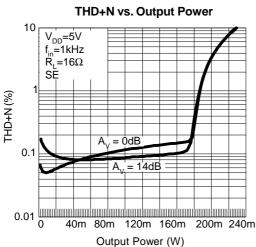


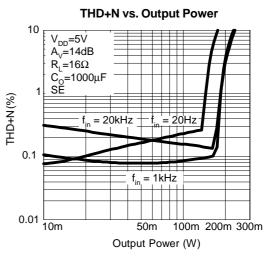


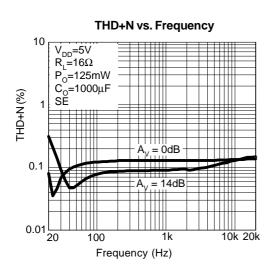


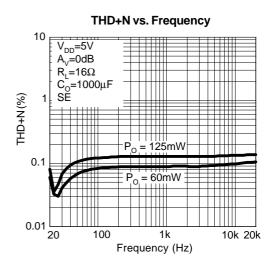




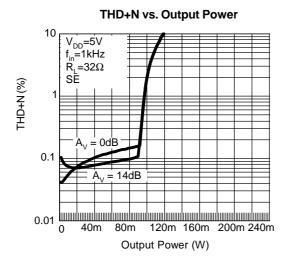


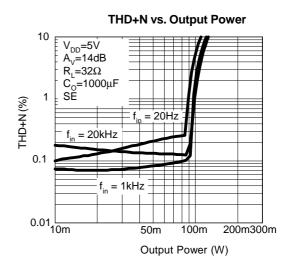


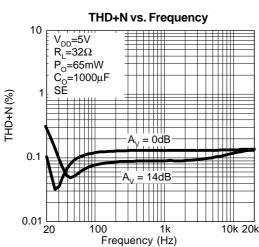


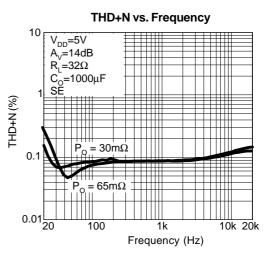


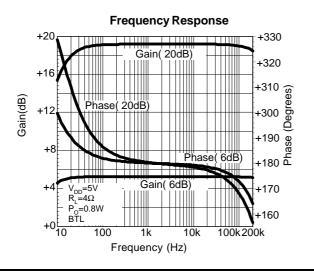


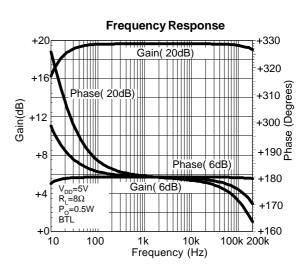




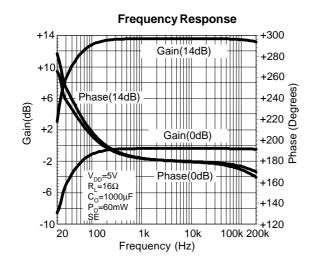


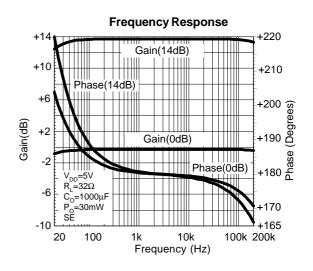


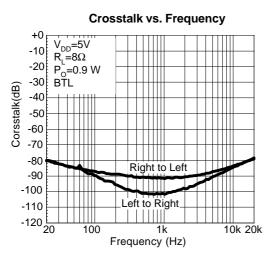


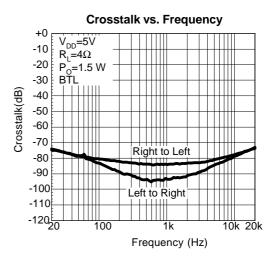


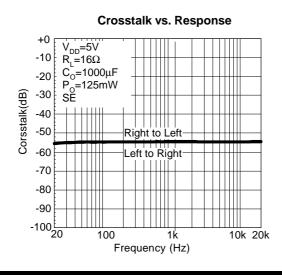


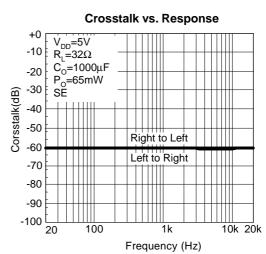




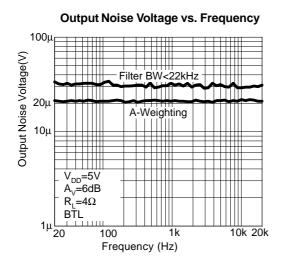


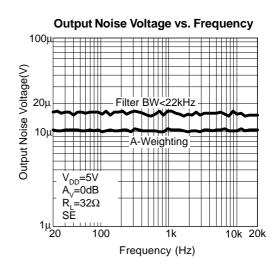


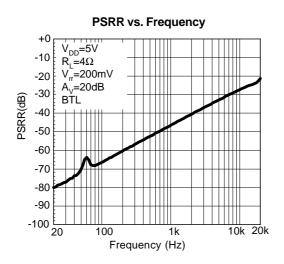


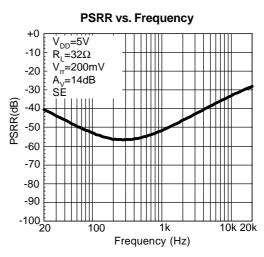


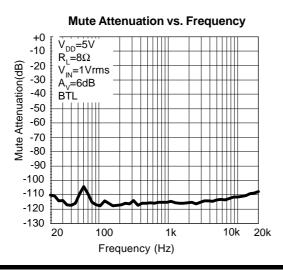


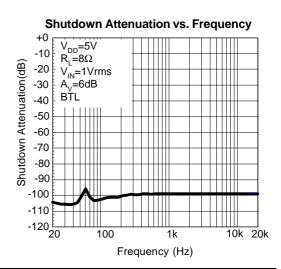




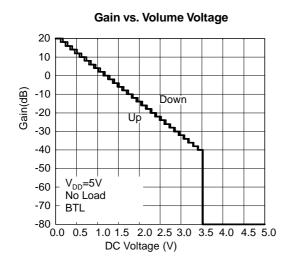


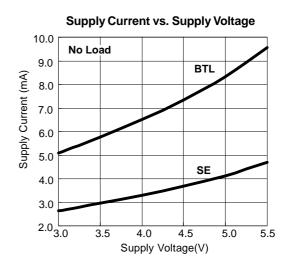


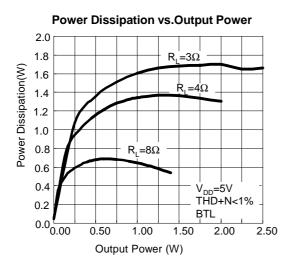


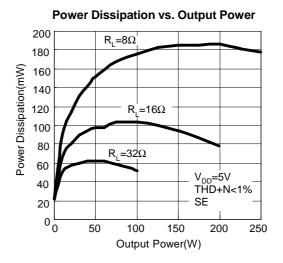














## **Application Information**

### **BTL Operation**

The APA2068 output stage (power amplifier) has two pairs of operational amplifiers internally, which allows different amplifier configurations.

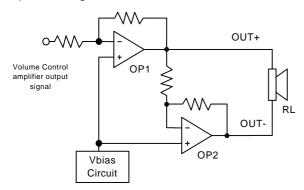


Figure 1: APA2068 Internal Configuration (each channel)

The power amplifier's OP1 gain is set by internal unity-gain and input audio signal comes from internal volume control amplifier while the second amplifier OP2 is internally fixed in a unity-gain, inverting configuration. Figure 1 shows that the output of OP1 is connected to the input to OP2, which results in the output signals of with both amplifiers with identical in magnitude but out of phase  $180^{\circ}$ . Consequently, the differential gain for each channel is  $2 \times (Gain of SE mode)$ .

By driving the load differentially through outputs OUT+ and OUT-, an amplifier configuration is commonly referred to bridged mode is established. BTL mode operation is different from the classical single-ended SE amplifier configuration where one side of its load is connected to the ground.

A BTL amplifier design has a few distinct advantages over the SE configuration, as it provides differential drive to the load, thus, doubles the output swing for aspecified supply voltage.

When placed under the same conditions, a BTL amplifier has four times the output power of a SE amplifier. A BTL configuration, such as the one used in APA2068, also creates a second advantage over SE amplifiers. Since the differential outputs, ROUT+, ROUT-, LOUT+, and LOUT-, are biased at half-supply, it's not necessary for DC voltage to be across the load. This eliminates the need for an output coupling capacitor which is required in

a single supply, SE configuration.

### **Single-Ended Operation**

To consider the single-supply SE configuration shown Application Circuit, a coupling capacitor is required to block the DC offset voltage from reaching the load. These capacitors can be quite large (approximately  $33\mu F$  to  $1000\mu F$ ), so they tend to be expensive, occupy valuable PCB area, and have the additional drawback of limiting low-frequency performance of the system (refer to the Output Coupling Capacitor). The rules described still hold with the addition of the following relationship:

$$\frac{1}{C_{\rm B} \times 150 \text{k}\Omega} \le \frac{1}{R_{\rm i}C_{\rm i}} << \frac{1}{R_{\rm i}C_{\rm c}} \tag{1}$$

### Output SE/BTL Operation

The best cost saving feature of APA2068 is that it can be switched easily between BTL and SE modes. This feature eliminates the requirement for an additional headphone amplifier in applications where internal stereo speakers are driven in BTL mode but external headphone or speakers must be accommodated.

Inside of the APA2068, two separate amplifiers drive OUT+ and OUT- (see Figure 1). The SE/BTL input controls the operation of the follower amplifier that drives LOUT- and ROUT-.

- When SE/BTL keeps low, the OP2 turns on and the APA2068 is in the BTL mode.
- When SE/BTL keeps high, the OP2 is in a high output impedance state, which configures the APA2068 as SE driver from OUT+. I<sub>DD</sub> is reduced by approximately onehalf in SE mode.

Control of the SE/BTL input can be a logic-level TTL source or a resistor divider network or the stereo headphone jack with switch pin as shown in the Application Circuit.



### Output SE/BTL Operation (Cont.)

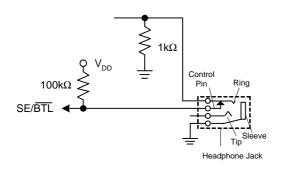


Figure 2: SE/BTL Input Selection by Phonejack Plug

In Figure 2, input SE/BTL operates as below:

When the phonejack plug is inserted, the  $1k\Omega$  resistor is disconnected and the SE/BTL input is pulled high and enables the SE mode. When the input goes high, the OUT- amplifier is shutdown causing the speaker to mute. The OUT+ amplifier then drives through the output capacitor ( $C_o$ ) into the headphone jack. When there is no headphone plugged into the system, the contact pin of the headphone jack is connected from the signal pin, the voltage divider set up by resistors  $100k\Omega$  and  $1k\Omega$ . Resistor  $1k\Omega$  then pulls low the SE/BTL pin, enabling the BTL function.

#### **Volume Control Function**

The APA2068 has an internal stereo volume control that setting is the function of the DC voltage applied to the VOLUME input pin. The APA2068 volume control consists of 32 steps that are individually selected by a variable DC voltage level on the VOLUME control pin. The range of the steps, controlled by the DC voltage, are from 20dB to -80dB. Each gain step corresponds to a specific input voltage range, as shown in table. To minimize the effect of noise on the volume control pin, which can affect the selected gain level, hysteresis and clock delay are implemented. The amount of hysteresis corresponds to half of the step width, as shown in the volume control graph.

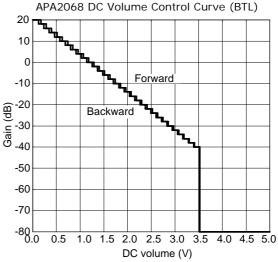


Figure 3: Gain Setting vs. VOLUME Pin Voltage

For the highest accuracy, the voltage shown in the 'recommended voltage' column of the table is used to select a desired gain. This recommended voltage is exactly half-way between the two nearest transitions. The gain levels are 2dB/step from 20dB to -40dB in BTL mode, and the last step at -80dB as mute mode.

#### Input Resistance, R.

The gain for each audio input of the APA2068 is set by the internal resistors ( $R_i$  and  $R_F$ ) of volume control amplifier in inverting configuration.

SE Gain = Av = 
$$-\frac{R_F}{R_i}$$
 (2)

BTL Gain = 
$$-2 \times \frac{R_F}{R_i}$$
 (3)

BTL mode operation brings the factor of 2 in the gain equation due to the inverting amplifier mirroring the voltage swing across the load. For varying gain settings, the APA2068 generates each input resistance on figure 4. The input resistance will affect the low frequency performance of audio signal. The minmum input resistance is  $10k\Omega$  when gain setting is 20dB and the resistance will ramp up when close loop gain below 20dB. The input resistance has wide variation (+/-10%) caused by process variation.



### Input Resistance, R, (Cont.)

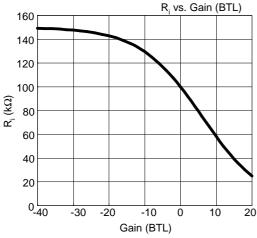


Figure 4: Input Resistance vs. Gain Setting

### Input Capacitor, C

In the typical application, an input capacitor,  $C_i$ , is required to allow the amplifier to bias the input signal to the proper DC level for optimum operation. In this case,  $C_i$  and the minimum input impedance  $R_i$  (25k $\Omega$ ) form a high-pass filter with the corner frequency determined in the following equation :

Fc(highpass) = 
$$\frac{1}{2\pi \times 25k\Omega \times C_i}$$
 (4)

The value of  $C_i$  is important to consider as it directly affects the low frequency performance of the circuit. Consider the example where  $R_i$  is  $25k\Omega$  and the specification calls for a flat bass response down to 50Hz. Equation is reconfigured as below :

$$C_{i} = \frac{1}{2\pi \times 25k\Omega \times F_{C}}$$
 (5)

When the input resistance variation is considered, the  $C_i$  is  $0.13\mu F$ , therefore, a value in the range of  $0.33\mu F$  to  $1.0\mu F$  would be chosen. A further consideration for this capacitor is the leakage path from the input source through the input network  $(R_i + R_F, C_i)$  to the load. This leakage current creates a DC offset voltage at the input to the amplifier that reduces useful headroom, especially in high gain applications. For this reason, a low-leakage tantalum or ceramic capacitor is the best choice. When polarized capacitors are used, the positive side of the capacitor should face the amplifier input in most applications because the DC level of the amplifiers' input is held at  $V_{DD}/2$ . Please note that it is important to confirm the capacitor

polarity in the application.

### Effective Bypass Capacitor, C<sub>B</sub>

A power amplifier, proper supply bypassing, is critical for low noise performance and high power supply rejection. The capacitor location on the BYPASS pin should be as close to the device as possible. The effect of a larger supply bypass capacitor is to improve PSRR due to increased half-supply stability. Two critical criteria of bypass capacitor ( $C_B$ ): 1st, it depends upon desired PSRR requirements and click-and-pop performance; 2nd, the leakage current of  $C_B$  will induce the voltage drop of  $V_{BYPASS}$  (voltage of BYPASS pin), and if the  $V_{BYPASS}$  is less than  $0.49V_{DD}$ , APA2068 will enter mute condition. The value of  $V_{BYPASS}$  can be calculated as below:

$$V_{\text{BYPASS}} = 0.5 V_{\text{DD}} - I_{\text{Leakage}} \times 150 k\Omega$$

#### Where

 $I_{Leakage}$  =Leakage current of  $C_{R}$ 

Therefore, it is recommended that  $C_{\text{B}}$ 's leakage current should be no more then 0.4 $\mu A$  for properly work of APA2068.

To avoid the start-up pop noise, the bypass voltage should rise slower than the input bias voltage and the relationship shown in equation should be maintained.

$$\frac{1}{(C_B X150k\Omega)} \ll \frac{1}{C_i X150k\Omega} \tag{7}$$

The capacitor is fed from a 150k $\Omega$  resistor inside of the amplifier and the 150k $\Omega$  is the maximum input resistance of (R<sub>i</sub>+R<sub>F</sub>). Bypass capacitor, C<sub>B</sub>, values of 2.2 $\mu$ F to 10 $\mu$ F ceramic or tantalum low-ESR capacitors are recommended for the best THD+N and noise performance. The bypass capacitance also affects the start up time. It is determined in the following equation:

Tstart up = 
$$5X(C_{BYPASS}X150k\Omega)$$
 (8)

### Output Coupling Capacitor, C<sub>c</sub>

In the typical single-supply SE configuration, an output coupling capacitor ( $C_{\rm C}$ ) is required to block the DC bias at the output of the amplifier thus preventing DC currents in the load. As with the input coupling capacitor, the output coupling capacitor and impedance of the load form a high-pass filter governed by the equation.

$$Fc(highpass) = \frac{1}{2\pi R \iota Cc}$$
 (9)



### Output Coupling Capacitor, Cc (Cont.)

For example, a 330µF capacitor with an  $8\Omega$  speaker would attenuate low frequencies below 60.6Hz. The main disadvantage, from a performance standpoint, is the load impedance and is typically small, which drives the low-frequency corner higher degrading the bass response. Large values of  $C_c$  are required to pass low frequencies into the load.

#### Power Supply Decoupling, Cs

The APA2068 is a high-performance CMOS audio amplifier that requires adequate power supply decoupling to ensure the output total harmonic distortion (THD+N) is as low as possible. Power supply decoupling also prevents the oscillations being caused by long lead length between the amplifier and the speaker. The optimum decoupling is achieved by using two different types of capacitors that target on different types of noise on the power supply leads.

For higher frequency transients, spikes, or digital hash on the line, a good low equivalent-series-resistance (ESR) ceramic capacitor, typically 0.1  $\mu\text{F}$ , is placed as close as possible to the device  $V_{\text{DD}}$  lead works best. For filtering lower-frequency noise signals, it is recommended to place a large aluminum electrolytic capacitor of  $10\mu\text{F}$  or greater near the audio power amplifier.

### **Optimizing Depop Circuitry**

Circuitry has been included in the APA2068 to minimize the amount of popping noise at power-up and when coming out of shutdown mode. Popping occurs whenever a voltage step is applied to the speaker. In order to eliminate clicks and pops, all capacitors must be fully discharged before turn-on. Rapid on/off switching of the device or the shutdown function will cause the click and pop circuitry.

The value of  $C_i$  will also affect turn-on pops (Refer to Effective Bypass Capacitance). The bypass voltage ramp up should be slower than input bias voltage. Although the bypass pin current source cannot be modified, the size of  $C_{\text{BYPASS}}$  can be changed to alter the device turn-on time and the amount of clicks and pops. By increasing the value of  $C_{\text{BYPASS}}$ , turn-on pop can be reduced. However, the tradeoff for using a larger bypass capacitor is to increase the turn-on time for this device. There is a linear relation-

ship between the size of  $C_{\rm BYPASS}$  and the turn-on time. In a SE configuration, the output coupling capacitor,  $C_{\rm C}$ , is of particular concern.

This capacitor discharges through the internal  $10 K\Omega$  resistors. Depending on the size of  $C_c$ , the time constant can be relatively large. To reduce transients in SE mode, an external  $1 k\Omega$  resistor can be placed in parallel with the internal  $10 k\Omega$  resistor. The tradeoff for using this resistor is an increase in quiescent current. In most cases, choosing a small value of  $C_i$  in the range of  $0.33 \mu F$  to  $1 \mu F$ , Cb being equal to  $4.7 \mu F$  and an external  $1 k\Omega$  resistor should be placed in parallel with the internal  $10 k\Omega$  resistor should produce a virtually clickless and popless turn-on.

A high gain amplifier intensifies the problem as the small delta in voltage is multiplied by the gain, so it is advantageous to use low-gain configurations.

#### **Shutdown Function**

In order to reduce power consumption when not in use, the APA2068 contains a shutdown pin to externally turn off the amplifier bias circuitry. This shutdown feature turns the amplifier off when a logic low is placed on the  $\overline{\rm SHUTDOWN}$  pin. The trigger point between a logic high and logic low level is typically 2.0V. It is best to switch between the ground and the supply  $\rm V_{DD}$  to provide maximum device performance.

By switching the  $\overline{SHUTDOWN}$  pin to low, the amplifier enters a low-current state,  $I_{DD} < 1\mu A$ . APA2068 is in shutdown mode. On normal operating,  $\overline{SHUTDOWN}$  pin pull to high level to keep the IC out of the shutdown mode. The  $\overline{SHUTDOWN}$  pin should be tied to a definite voltage to avoid unwanted state changing.

### **Mute Function**

The APA2068 mutes the amplifier outputs when logic high is applied to the MUTE pin. Applying logic low to the MUTE pin returns the APA2068 to normal operation. Prevent unanticipated mute behavior by connecting the Mute pin to logic high or low. Do not let the Mute pin float.



### **Maximum Output Swing Clamping Function (VolMax)**

The APA2068 provides the maximum output swing clamping function to protect the speaker.

When input a non-zero voltage ( $V_x$ ) to VolMax pin, the amplifier's output amplitude ( $V_o$ ) is be limited at  $V_o = V_{DD} - V_x$ . This function can effectively limite the output power across the speaker and avoid damaging the speaker.

The maximum setting voltage of VolMax is Vdd/2, and when this function is not used, connect the VolMax to the GND.

#### **BTL Amplifier Efficiency**

An easy-to-use equation to calculate efficiency starts out as being equal to the ratio of power from the power supply to the power delivered to the load.

The following equations are the basis for calculating amplifier efficiency.

$$Efficiency = \frac{1}{P_{SUP}}$$
 (10)

Where

$$P_O = \frac{V_{orms} \times V_{orms}}{R_L} = \frac{(V_P \times V_P)}{2R_L}$$

$$V_{orms} = \frac{V_P}{\sqrt{2}} \tag{11}$$

$$P_{SUP} = V_{DD} \times L_{DDSVG} = V_{DD} \times \frac{2V_P}{\pi R_I}$$
 (12)

Efficiency of a BTL configuration:

$$\frac{P_{O}}{P_{SUP}} = \frac{\left(\frac{V_{P} \times V_{P}}{2R_{L}}\right)}{\left(V_{DD} \times \frac{2V_{P}}{\pi R_{L}}\right)} = \frac{\pi V_{P}}{4V_{DD}}$$
(13)

Table 1 calculates efficiencies for four different output power levels.

Note that the efficiency of the amplifier is quite low for lower power levels and rises sharply as power to the load is increased resulting in a nearly flat internal power dissipation over the normal operating range.

Note that the internal dissipation at full output power is less than in the half power range. Calculating the efficiency for a specific system is the key to proper power supply design. For a stereo 1W audio system with  $8\Omega$  loads and a 5V supply, the maximum draw on the power supply is almost 3W.

A final point to remember about linear amplifiers (either SE or BTL) is how to manipulate the terms in the efficiency equation to utmost advantage when possible. Note that in equation,  $V_{DD}$  is in the denominator. This indicates that as  $V_{DD}$  goes down, efficiency goes up. In other words, use the efficiency analysis to choose the correct supply voltage and speaker impedance for the application.

Po (W)	Efficiency (%)	I <sub>DD</sub> (A)	V <sub>PP</sub> (V)	P <sub>D</sub> (W)
0.25	31.25	0.16	2.00	0.55
0.50	47.62	0.21	2.83	0.55
1.00	66.67	0.30	4.00	0.5
1.25	78.13	0.32	4.47	0.35

<sup>\*\*</sup>High peak voltages cause the THD+N to increase.

Table 1. Efficiency vs. Output Power in 5-V/8 $\Omega$  BTL Systems

#### **Power Dissipation**

Whether the power amplifier is operated in BTL or SE mode, power dissipation is the major concern. Equation14 states the maximum power dissipation point for a SE mode operating at a given supply voltage and driving a specified load.

SE mode: P<sub>D,MAX</sub> = 
$$\frac{V_{DD}^2}{2\pi^2 R_L}$$
 (14)

In BTL mode operation, the output voltage swing is doubled as in SE mode. Thus, the maximum power dissipation point for a BTL mode operating at the same given conditions is 4 times as in SE mode.

BTL mode: P<sub>D,MAX</sub> = 
$$\frac{4V_{DD}^2}{2\pi^2R_L}$$
 (15)

Since the APA2068 is a dual channel power amplifier, the maximum internal power dissipation is 2 times that both of equations depend on the mode of operation. Even with this substantial increase in power dissipation, the APA2068 does not require extra heatsink. The power dissipation from equation14, assuming a 5V-power supply and an  $8\Omega$  load, must not be greater than the power dissipation that results from the equation16:

$$P_{D, MAX} = \frac{T_{J, MAX} - T_{A}}{\theta_{JA}}$$



#### **Power Dissipation (Cont.)**

For SOP16-P package with thermal pad, the thermal resistance ( $\theta_{JA}$ ) is equal to 45°C/W.

Since the maximum junction temperature  $(T_{J,MAX})$  of APA2068 is 150°C and the ambient temperature  $(T_A)$  is defined by the power system design, the maximum power dissipation which the IC package is able to handle can be obtained from equation16.

Once the power dissipation is greater than the maximum limit ( $P_{D,MAX}$ ), either the supply voltage ( $V_{DD}$ ) must be decreased, the load impedance ( $R_L$ ) must be increased or the ambient temperature should be reduced.

#### **Thermal Pad Consideration**

The thermal pad must be connected to the ground. The package with thermal pad of the APA2068 requires special attention on thermal design. If the thermal design issues are not properly addressed, the APA2068  $4\Omega$  will go into thermal shutdown when driving a  $4\Omega$  load.

The thermal pad on the bottom of the APA2068 should be soldered down to a copper pad on the circuit board. Heat can be conducted away from the thermal pad through the copper plane to ambient. If the copper plane is not on the top surface of the circuit board, 8 to 10 vias of 13 mil or smaller in diameter should be used to thermally couple the thermal pad to the bottom plane.

For good thermal conduction, the vias must be plated through and solder filled. The copper plane used to conduct heat away from the thermal pad should be as large as practical.

If the ambient temperature is higher than 25°C, a larger copper plane or forced-air cooling will be required to keep the APA2068 junction temperature below the thermal shutdown temperature (150°C). In higher ambient temperature, higher airflow rate and/or larger copper area will be required to keep the IC out of thermal shutdown.

#### **Thermal Consideration**

Linear power amplifiers dissipate a significant amount of heat in the package under normal operating conditions. To calculate maximum ambient temperatures, first consideration is that the numbers from the **Power Dissipation vs. Output Power** graphs are per channel values, so the dissipation of the IC heat needs to be doubled for two-channel operation. Given  $\theta_{JA}$ , the maximum allowable junction temperature  $(T_{JMAX})$ , and the total internal dissipation  $(P_D)$ , the maximum ambient temperature can be calculated with the following equation. The maximum recommended junction temperature for the APA2068 is 150°C. The internal dissipation figures are taken from the **Power Dissipation vs. Output Power** graphs.

$$T_{AMax} = T_{JMax} - \theta_{JA} P_{D}$$

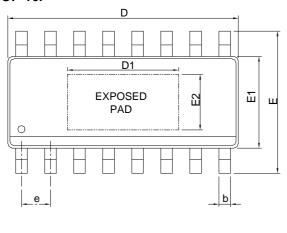
$$150 - 45(0.8*2) = 78°C$$
(16)

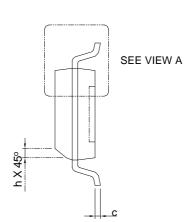
The APA2068 is designed with a thermal shutdown protection that turns the device off when the junction temperature surpasses 150°C to prevent damaging the IC.

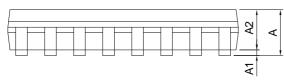


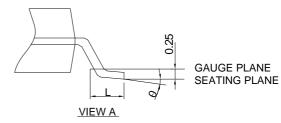
# **Package Information**

## SOP-16P









S	SOP-16P						
S Y M B O L	MILLIMI	ETERS	INCHES				
, p	MIN.	MAX.	MIN.	MAX.			
А		1.75		0.069			
A1	0.00	0.15	0.000	0.006			
A2	1.25		0.049				
b	0.31	0.51	0.012	0.020			
С	0.17	0.25	0.007	0.010			
D	9.80	10.00	0.386	0.394			
D1	3.50	4.50	0.138	0.177			
E	5.80	6.20	0.228	0.244			
E1	3.80	4.00	0.150	0.157			
E2	2.00	3.00	0.079	0.118			
е	1.27 BSC		0.05	0 BSC			
h	0.25	0.50	0.010	0.020			
L	0.40	1.27	0.016	0.050			
θ	0°	8°	0°	8°			

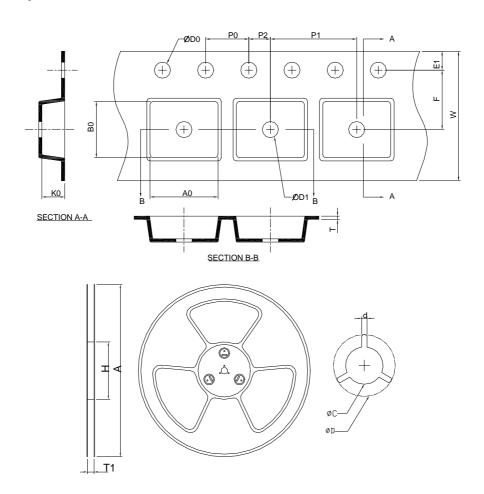
Note: 1. Follow from JEDEC MS-012 BC.

- 2. Dimension "D" does not include mold flash, protrusions or gate burrs. Mold flash, protrusion or gate burrs shall not exceed 6 mil per side.
- 3. Dimension "E" does not include inter-lead flash or protrusions.

  Inter-lead flash and protrusions shall not exceed 10 mil per side.



# **Carrier Tape & Reel Dimensions**



<b>Application</b>	Α	Н	T1	С	d	D	W	E1	F
	330.0 ±2.00	50 MIN.	16.4+2.00 -0.00	13.0+0.50 -0.20	1.5 MIN.	20.2 MIN.	16.0 <b>±</b> 0.30	1.75 <b>±</b> 0.10	7.5 <b>±</b> 0.10
SOP-16P	P0	P1	P2	D0	D1	T	A0	B0	K0
	4.0 <b>±</b> 0.10	8.0 ±0.10	2.0 ±0.10	1.5+0.10 -0.00	1.5 MIN.	0.6+0.00 -0.40	6.40 ±0.20	10.30 <b>±</b> 0.20	2.10 <b>±</b> 0.20

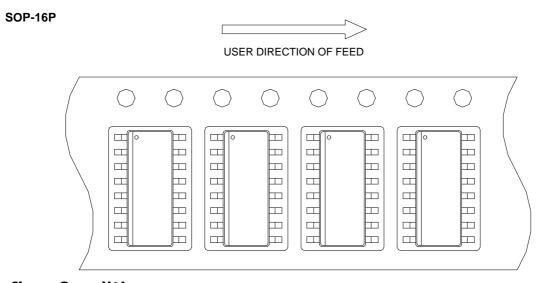
(mm)

## **Devices Per Unit**

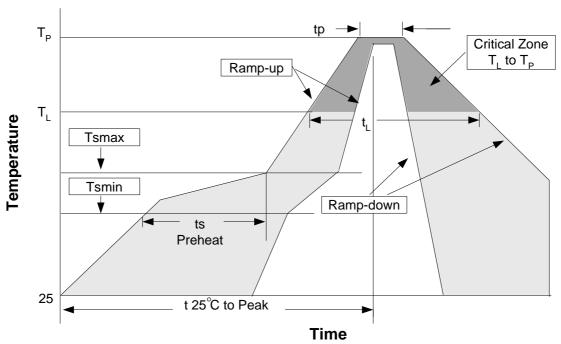
Package Type	Unit	Quantity
SOP-16P	Tape & Reel	2500



# **Taping Direction Information**



# Reflow Condition (IR/Convection or VPR Reflow)



## **Reliability Test Program**

Test item	Method	Description
SOLDERABILITY	MIL-STD-883D-2003	245°C, 5 sec
HOLT	MIL-STD-883D-1005.7	1000 Hrs Bias @125°C
PCT	JESD-22-B, A102	168 Hrs, 100%RH, 121°C
TST	MIL-STD-883D-1011.9	-65°C~150°C, 200 Cycles
ESD	MIL-STD-883D-3015.7	VHBM > 2KV, VMM > 200V
Latch-Up	JESD 78	$10ms, 1_{tr} > 100mA$



## **Classification Reflow Profiles**

Profile Feature	Sn-Pb Eutectic Assembly	Pb-Free Assembly
Average ramp-up rate (T <sub>L</sub> to T <sub>P</sub> )	3°C/second max.	3°C/second max.
Preheat - Temperature Min (Tsmin) - Temperature Max (Tsmax) - Time (min to max) (ts)	100°C 150°C 60-120 seconds	150°C 200°C 60-180 seconds
Time maintained above: - Temperature (T <sub>L</sub> ) - Time (t <sub>L</sub> )	183°C 60-150 seconds	217°C 60-150 seconds
Peak/Classification Temperature (Tp)	See table 1	See table 2
Time within 5°C of actual Peak Temperature (tp)	10-30 seconds	20-40 seconds
Ramp-down Rate	6°C/second max.	6°C/second max.
Time 25°C to Peak Temperature	6 minutes max.	8 minutes max.

Note: All temperatures refer to topside of the package. Measured on the body surface.

Table 1. SnPb Eutectic Process – Package Peak Reflow Temperatures

Package Thickness	Volume mm <sup>3</sup> <350	Volume mm <sup>3</sup> <sup>3</sup> 350
<2.5 mm	240 +0/-5°C	225 +0/-5°C
≥2.5 mm	225 +0/-5°C	225 +0/-5°C

Table 2. Pb-free Process – Package Classification Reflow Temperatures.

Package Thickness	Volume mm <sup>3</sup> <350	Volume mm <sup>3</sup> 350-2000	Volume mm <sup>3</sup> >2000
<1.6 mm	260 +0°C*	260 +0°C*	260 +0°C*
1.6 mm – 2.5 mm	260 +0°C*	250 +0°C*	245 +0°C*
≥2.5 mm	250 +0°C*	245 +0°C*	245 +0°C*

<sup>\*</sup>Tolerance: The device manufacturer/supplier **shall** assure process compatibility up to and including the stated classification temperature (this means Peak reflow temperature +0°C. For example 260°C+0°C) at the rated MSL level.

## **Customer Service**

## **Anpec Electronics Corp.**

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